## APPENDIX I

## REFERENCES USED TO DEVELOP THE TRAMAN

**NOTE:** The following references were current at the time this TRAMAN was published, but you should be sure you have the current edition.

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## **APPENDIX II**

## **USEFUL TABLES**

Table AII-1.—Natural Sines and Cosines

M	0.	1*	2-	3*	4.
н 7	SIN COS	SIN COS	SIN COS	SIN COS	SIN COS
0					1 0.06976 1 0.99756 1 60
2 1		0.01774 ! 0.99984 !			
	0.00087   1.00000	0.01803   0.99984	0.03348   0.77737	0.05292   0.99860	0.07034   0.99752   58     0.07063   0.99750   57
4 1		0.01862   0.99983			
	0.00145   1.00000	0.01891   0.99982	0.03635   0.99934	0.05379   0.99855	1 0.07121 1 0.99746 1 55
	0.00175   1.00000	0.01920   0.99982	0.03664   0.99933	0.05408   0.99854	1 0.07150   0.99744   54
7 I 8 I		0.01949   0.99981	0.03693   0.99932	0.05437   0.99852	1 0.07179   0.99742   53
9	0.00253   1.00000	0.01978   0.99980     0.02007   0.99980	0.03/23   0.99931	0.05466   0.99851	1 0.07208   0.99740   52
		0.02036   0.99979			
		0.02065   0.99979			
12	0.00349   0.99999	0.02094   0.99978	0.03839   0.99926	1 0.05582 1 0.99844	1 0.07324   0.99731   48
13 1	0.00378   0.99999	0.02123   0.99977	0.03868   0.99925	0.05611   0.99842	1 0.07353   0.99729   47
14	0.00407   0.99999	0.02152   0.99977	0.0 <b>38</b> 97   0.99924	0.05640   0.99841	1 0.07382   0.99727   46
	0.00436   0.99999     0.00465   0.99999	0.02181   0.99976	0.03926   0.99923	0.05667   0.99839	1 0.07411   0.99725   45
	0.00485   0.99999	0.02211   0.99976     0.02240   0.99975	0.03733   0.77722	1 0.05678   0.77838	1 0.07440   0.99723   44
	0.00524   0.99999				
19	0.00553   0.99998	0.02298   0.99974	0.04042   0.99918	0.05785   0.99833	1 0.07527 1 0.99716 1 41
20	0.00582   0.99998	0.02327   0.99973	0.04071   0.99917	0.05814   0.99831	1 0.07556 1 0.99714 1 40
21	0.00611   0.9999B	0.02356   0.99972	0.04100   0.99916	0.05844   0.99829	0.07585   0.99712   39
22	0.00640   0.99998	0.02385   0.99972	0.04129   0.99915	0.05873   0.99827	1 0.07614   0.99710   38
24	0.00669   0.99998     0.00698   0.99998	0.02414   0.444/1	0.04159   0.99913	0.05902   0.99826	0.07643   0.99708   37
25	0.00727   0.99997	0.02472   0.99969	1 0.04217 1 0.99911	1 0.05751   0.77824	0.07672   0.99705   36   0.07701   0.99703   35
26	0.00756 1 0.99997	0.02501   0.99969	0.04246   0.99910	0.05789   0.99821	1 0.07730   0.77703   33
27	0.00785   0.9 <del>99</del> 97	0.02530   0.9 <del>9</del> 948	1 0.04275 I 0.99909	0.06018   0.99819	1 0.07759   0.99699   33
28	0.00814   0.99997	0.02560   0.99967	0.04304   0.99907	1 0.06047 1 0.99817	1 0.07788 1 0.99696 1 32
29	0.00844   0.99996	1 0.025B9   0.99966	1 0.04333   0.99906	1 0.04074 1 0.99815	1 0.07817 1 0.99694 1 31
30	0.00873   0.99996	1 0.02618   0.77766	1 0.04362   0.44405	0.06105   0.99813	1 0.07846 1 0.99692 1 30
32	0.00931   0.99996	0.02676   0.99964	0.04420   0.99902	1 0.06163   0.77812	1 0.07875   0.99689   29 1 0.07904   0.99687   28
22	0.00960   0.99995	1 0.02705   0.99963	0.04449-  0.99901	1 0.06192   0.99808	1 0.07933 1 0.99685 1 27
34	0.00989   0.99995	1 0.02734 1 0.99963	1 0.04478   0.99900	1 0.06221   0.99806	1 0.07962 1 0.99683 1 26
35	0.01018   0.99995	1 0.02763 1 0.99962	1 0.04507   0.99898	1 0.06250 1 0.99804	1 0.07991 1 0.99680 1 25
77	0.01047   0.99995 0.01076   0.99994	0.02792   0.99961	1 0.04536   0.99897	1 0.06279 1 0.99803	1 0.08020   0.99678   24
38	0.01105   0.99994	1 0.02850 1 0.99959	1 0.04584   0.99894	1 0.06308   0.77801	1 0.08049 1 0.99676 1 23
39	0.01134   0.99994	0.02879   0.99959	1 0.04623 1 0.99893	1 0.06366 1 0.99797	1 0.08107 1 0.99671 1 21
40	0.01164   0.99993	0.02908   0.99958	1 0.04653 1 0.99892	1 0.06395 1 0.99795	1 0.08136 1 0.99668 1 20
41	1 0.01193   0.99993	1 0.02938 1 0.99957	1 0.04682   0.99890	1 0.06424   0.99793	1 0.08165   0.99666   19
42	0.01222   0.99993	1 0.02967   0.99956	1 0.04711   0.99889	1 0.06453 1 0.99792	1 0.08194   0.99664   18
44	0.01251   0.99992	1 0.03025 1 0.99954	1 0.04740   0.97888	1 0.06482   0.99790	1 0.08223   0.99661   17
	1.0.01309   0.99991	1 0.03054 1 0.99953	1 0.04798 1 0.99885	1 0.06540 1 0.99788	1 0.08252   0.99659   16
46	1 0.01338   0.99991	1 0.03083   0.99952	1 0.04827 1 0.99883	1 0.06569 1 0.99784	1 0.08310 1 0 99454 1 14
47	0.01367   0.99991	0.03112   0.99952	1 0.04856 1 0.99892	1 0.06598 1 0.99782	1 0 08779 1 0 99452 1 17
48	0.01396   0.99990	1 0.03141   0.99951	1 0.04885 1 0.99881	1 0.06627 1 0.99780	1 0.08368 L 0.99649 L 12
50	0.01425   0.99990     0.01454   0.99990	1 0.03170 1 0.99950	1 0.04914 1 0.99879	1 0.06656 1 0.99778	1 0.08397 1 0.99647 1 11.
51	1 0.01483   0.99989	1 0.03228 1 0.99948	1 0.04743   0.448/8	1 0.00083   0.99776	1 0.08426   0.99644   10
	1 0.01513   0.99989	I 0.03257 I 0.99947	1 0.05001   0.99875	1 0.06743 1 0.99772	1 0.08484   0.99639   8
53	1 0.01542   0.99988	1 0.03286 1 0.99946	1 0.05030 1 0.99873	1 0.06773 1 0.99770	1 0 08513 1 0 88437 1 7
54	1 0.01571   0.99988	1 0.03316   0.99945	1 0.05059 1 0.99872	1 0.06802 1 0.99768	1 0.08542   0.99635   A
55	0.01400   0.99987	1 0.03345   0.99944	1 0.05088 1 0.99870	1 0.04831 1 0.99766	1 0.08571   0.99632   5
57	1 0.01658 1 0.99984	1 0.033/4   0.77743	1 0.05144   0.99847	1 0.06860 1 0.99764	1 0.08600   0.99630   4
1 28	1 0.01687   0.99986	1 0.03432   0.99941	1 0.05175 I 0.99844	1 0.06918 1 0.99760	1 0.08A58 1 0.99A25 1 2
1 24	1 0.01716   0.99985	1 0.03461   0.99940	1 0.05205   0.99864	1 0.06947 1 0.9975B	1 0 08687 1 0 99622 1 1
60	1 0.01745 1 0.99985	1 0.03490 1 0.99939	1 0.05234 1 0.99863	1 0.06976 1 0.99756	1 0.08716   0.99619   0
	COS SIN	COS SIN	COS SIN	COS SIN	COS SIN M
{					r
1	89*	88*	87*	86*	85. Y

**Table AII-1.—Natural Sines and Cosines—Continued** 

M	5	-	6	-	フ	•	8	•	9	•	_
1 7	SIN	cos	SIN	cos	SIN	COS	SIN	cos	SIN	cos	
	0.08716 1										
1 1	0.08745 I	0.99617	0.10482 I	0.99449 1	0.12216	0.99251	0. 13946	0.99023	0.15672	0.98764	1 59
2 1	0.08774 1	0.99614 1	0.10511 1	0.99446 1	0.12245	0.99248	0.13975	0.99019	0.15701	0.98760	1 58
3 !	0.08821	0.99612	0.10540	0.99443	0.12274	0.99244	0.14004	0.99015	0.13730     0.15750	0.76755	3/
3 1	0.08840	0.99607	0.10567	0.99437	0.12331	0.77237	0.14041	0.99004	1 0. 15787 I	0.98744	55
	0.08889										
7 1	0.08918	0.99602	0.10655 1	0.99431 1	0.12389	0.99230	0.14119	0.78978	1 0.15845	0.98737	1 53
	0.08947										
	0.08976 1										
	0.09005 1										
	0.09034 1										
	0.07083 1										
	0.07072										
	0.09150										
	0.09179 1										
17 I	0.09208 1	0.99575	0.10945	0.99399	0.12678	0.99193	0.14407	0.98957	1 0.16132	0.98690	1 43
	0.09237 1										
	0.09266										
	0.09295										
	0.09324										
	0.09382 (										
	0.09411										
	0.09440 1										
	0.09469 1										
27:1	0.09498	0.99548	0.11234	0.99367	0.12966	0.99156	1 0.14695	0.98914	1 0.16419	0.98643	1 33
	0.09527										
	0.09556										
	0.09585										
	0.09614										
	0.09671										
	0.09700 I										
35 1	0.09729 !	0.99526	0.11465	0.99341	0.13197	0.99125	1 0.14925	0.78880	1 0.16648	0.98604	1 25
	0.09758										
	0.09787										
	0.09816										
	0.09845     0.09874										
	0.09903										
	0.09932										
	0.09961										
	0.09990										
	0.10019										
	0.10048										
	0.10077     0.10106										
	0.10135										
	0.10164										
51	0.10192	0.99479	0.11927	0.99286	1 0.13658	1 0.99063	1 0.15385	1 0.78809	1 0.17107	1 0.98526	1 9
52	0.10221	0.99476	0.11956	0.99283	0.13687	1 0.99059	1 0.15414	1 0.98805	1 0.17136	1 0.98521	1 8
	0.10250										
	0.10279	0.99470	0.12014	1 0.99276	1 0.13744	1 0.99051	1 0.15471	1 0.98794	1 0.17193	0.98511	1 6
55									1 0.17222		
57	0.10337 0.10366	1 0.77464 1 0.99441	1 0.120/1	1 0.77207	1 0.13802	1 0.77043	1 0.13329	1 0.78/87	1 0.17250	1 0. Y8501	1 4
	0.10395										
59	0.10424	0.99455	0.12158	0.99258	0.13889	1 0.99031	1 0.15615	1 0.98773	I 0. 17334	0.98484	1 1
60	0.10453	0.99452	1 0.12187	1 0.99255	1 0.13917	1 0.99027	1 0.15643	1 0.98769	1 0.17365	0.98481	iċ
	cos	SIN	cos	SIN	cos	SIN	cos	SIN	cos	SIN	
	84		8:		8:	- <b></b>	: 8		80		- :

**Table AII-1.—Natural Sines and Cosines—Continued** 

	10								14		
7 -	SIN	cos	SIN	cos	SIN	cos	SIN	cos	SIN	cos	•
01	0.17365	0.98481 1	0.19081	0.98163 1	0.20791 1	0.97815 1	0.22495 1	0.97437	0.24192	0.97030	60
1 (	0.17393	0.98476	0.19109	0.98157	0.20820	0.97809 1	0.22523	0.97430	0.24220	0.97023 1	59
2 !	0.17422	0.98471 !	0.19138	0.98152	0.20848	0.97803	0.22552	0.97424	0.24249	0.97015	58
					0.20877 i 0.20905 i						
					0.20733 1						
					0.20762						
					0.20990 1						
8 1	0.17594	0.98440	0.19309 1	0.98118	0.21019	0.97766	0.22722	0.97384	0.24418	0.96973	52
					0.21047						
					0.21076						
					0.21104						1 49
					0.21132     0.21161						
					0.21187						1 46
					0.21218						
					0.21246.1						
17 I	0.17852 I	0.98394	0.19566	0.98067	I 0.21275 I	0.97711	0.22977	0.97325	1 0.24672	0.96909	1 43
					0.21303						
					0.21331						
					0.21360						
					0.21388     0.21417						
					0.21417						
					1 0.21474 I						
					0.21502						
					0.21530						
					0.21559						
					1 0.21587						
					0.21616						
					0.21644						
					1 0.21672   1 0.21701						
					1 0.21701						
					0.21758						
35 i	0.18367	0.98299	0.20079	1 0.97963	0.21786	0.97598	1 0.23486	1 0.97203	1 0.25179	I 0.96778	1 25
					1 0.21814						
					0.21843						
					1.0.21871						1 22
					1.0.21899						
					1 0.21928 1 0.21956						
					1 0.21756						
					0.22013						
					1 0.22041						
					1 0.22070						
					1 0.22098						
					0.22126						
					0.22155						
					0.22183						
					1 0.22212						
					0.22248						
					1 0.22297						
54 1	0.18910	0.98196	1 0.20620	1 0.97851	1 0.22325	1 0.97476	1 0.24023	1 0.97072	1 0.25713	1 0.96638	1 6
					0.22353						
					0.22382						
					1 0.22410						
					1 0.22438						
					1 0.22495						
	cos	SIN	cos	SIN	cos	SIN	cos	SIN	cos	SIN	
	75	> -	78	<b>3</b> •	77	7 <b>-</b>	7.	<b>5</b> -	7:	5-	

Table AII-1.—Natural Sines and Cosines—Continued

0   0.25 1   0.25 2   0.25 3   0.25 5   0.26 6   0.26 7   0.26 8   0.26 9   0.26 10   0.26 11   0.26 12   0.26	882   0 938   0 946   0 974   0 974   0 077   0 050   0 107   0 135   0 143   0 141   0 217   0 247   0 303   0	. 96585   . 96578   . 96570   . 965655   . 96547   . 96540   . 96532   . 96524   . 96517   . 96502   . 965	0.27564   0.27592   0.27676   0.27676   0.27676   0.27704   0.27707   0.27787   0.27787   0.27815   0.27817   0.27871   0.27871   0.27871   0.27871	0.96126 0.96118 0.96102 0.96102 0.96094 0.96098 0.96078 0.96070 0.96062 0.96054 0.960554 0.96054 0.96054 0.96054	0.29265   0.29293   0.29321   0.29348   0.29346   0.29460   0.29460   0.29487   0.2948	0.95630 1 0.95622 1 0.95613 1 0.95613 1 0.95596 1 0.95599 1 0.95579 1 0.95571 1 0.95562	1 0.30929 1 0.30957 1 0.30985 1 0.31012 1 0.31040 1 0.31068 1 0.31095 1	0.95106 0.95097 0.95088 0.95079 0.95079 0.95061 0.95052	0.32584   0.32612   0.32639   0.32667   0.32667   0.32694   0.32722   0.32749	0.94552 0.94542 0.94533 0.94523 0.94523 0.94504	59   58   57   56   55   54
0   0.25 1   0.25 2   0.25 3   0.25 5   0.26 6   0.26 7   0.26 8   0.26 9   0.26 10   0.26 11   0.26 12   0.26	882   0 938   0 946   0 974   0 974   0 077   0 050   0 107   0 135   0 143   0 141   0 217   0 247   0 303   0	.96593   .96593   .96595   .96570   .96562   .96555   .96547   .96540   .96532   .96532   .96517   .96507   .96509   .96509	0.27564   0.27592   0.27620   0.27620   0.27648   0.27674   0.27731   0.27759   0.27787   0.27843   0.27843   0.27871   0.27899	0.96126 0.96118 0.96110 0.96102 0.96094 0.96096 0.96070 0.96070 0.96062 0.96034 0.96046 0.96046	029237 0.29265 0.29265 0.29321 0.29328 0.29376 0.29404 0.29432 0.29460 0.29487	1 0.95630 1 0.95622 1 0.95613 1 0.95605 1 0.95596 1 0.95596 1 0.95579 1 0.95571	0.30902     0.30929     0.30957     0.30957     0.31012     0.31040     0.31046     0.31095	0.95106 0.95097 0.95088 0.95079 0.95070 0.95061 0.95052	0.32557 0.32584 0.32612 0.32639 0.32667 0.32694 0.32722 0.32749	0.94552 0.94542 0.94533 0.94523 0.94514 0.94504	59   58   57   56   55   54
1   0.25 2   0.25 3   0.25 4   0.25 5   0.26 6   0.26 7   0.26 8   0.26 9   0.26 10   0.26 11   0.26 12   0.26	910   0 938   0 966   0 994   0 0022   0 0050   0 107   0 1135   0 1433   0 1431   0 1441   0 1	. 96585   . 96578   . 96578   . 96562   . 96555   . 96547   . 96547   . 96547   . 96517   . 96509   . 96592   . 96494   . 9649	0.27592   0.27620   0.27648   0.27676   0.27704   0.27731   0.27787   0.27787   0.278815   0.278813   0.278871   0.278871   0.278871   0.27899   10.278999	0.76118   0.76110   0.76102   0.76074   0.76086   0.76076   0.76070   0.76076   0.7607	0.29265   0.29293   0.29321   0.29348   0.29346   0.29460   0.29460   0.29487   0.2948	1 0.95622 1 0.95613 1 0.95605 1 0.95596 1 0.95598 1 0.95579 1 0.95571 1 0.95562	1 0.30929 1 0.30957 1 0.30985 1 0.31012 1 0.31040 1 0.31068 1 0.31095 1	0.95097   0.95088   0.95079   0.95070   0.95061   0.95052	0.32584   0.32612   0.32639   0.32667   0.32667   0.32694   0.32722   0.32749	0.94542 0.94533 0.94523 0.94514 0.94504	59   58   57   56   55   54
2   0.25 3   0.25 4   0.26 5   0.26 6   0.26 8   0.26 9   0.26 10   0.26 11   0.26 12   0.26	938   0 966   0 994   0 922   0 050   0 079   0 107   0 135   0 163   0 171   0 219   0 247   0 303   0	.96578   .96570   .96562   .96555   .96547   .96540   .96532   .96524   .96517   .96509   .96502   .96494   .96	0.27620   0.27648   0.27676   0.27704   0.27731   0.27757   0.27787   0.27815   0.27813   0.27871   0.27871   0.27871   0.27879   10	0.96110 1 0.96102 1 0.96094 1 0.96086 1 0.96078 1 0.96078 1 0.96062 1 0.96054 1 0.96046 1	0.29293   0.29321   0.29348   0.29376   0.29404   0.29432   0.29460   0.29487	1 0.95613 1 0.95605 1 0.95596 1 0.95588 1 0.95579 1 0.95571 1 0.95562	I 0.30957   0.30985   0.30985   0.31012   0.31040   0.31068   0.31095   0.31005   0.31005   0.31005   0.31005   0.31	0.95088 0.95079 0.95070 0.95061 0.95052	0.32612   0.32639   0.32667   0.32694   0.32722   0.32749	0.94533 0.94523 0.94514 0.94504 0.94495	1 58 1 57 1 56 1 55 1 54
3   0.25 4   0.25 5   0.26 6   0.26 7   0.26 8   0.26 10   0.26 11   0.26 12   0.26	966   0 994   0 022   0 050   0 079   0 107   0 135   0 163   0 191   0 219   0 247   0 275   0 303   0	. 96570   1	0.27648   0.27676   0.27704   0.27731   0.27757   0.27787   0.27815   0.27843   0.27843   0.27871   0.27879   0.2787	0.96102 i 0.96094 i 0.96086 i 0.96078 i 0.96070 i 0.96062 i 0.96064 i	0.29321 0.29348 0.29376 0.29376 0.29404 0.29432 0.29460 0.29487	1 0.95605 1 0.93596 1 0.93588 1 0.93579 1 0.93571 1 0.93562	1 0.30985   1 0.31012   1 0.31040   1 0.31068   1 0.31095	0.95079 0.95070 0.95061 0.95052	0.32639 0.32667 0.32694 0.32722 0.32749	0.94523 0.94514 0.94504 0.94495	1 57 1 56 1 55 1 54
4   0.25 5   0.26 6   0.26 7   0.26 8   0.26 9   0.26 10   0.26 11   0.26 12   0.26	994   0 022   0 050   0 079   0 107   0 135   0 163   0 191   0 219   0 247   0 275   0	. 96562   1 . 96555   1 . 96547   1 . 96540   1 . 96524   1 . 96517   1 . 96502   1 . 96502   1 . 96494   1	0.27676   0.27704   0.27704   0.27731   0.27759   0.277815   0.27815   0.27843   0.27871   0.27899   1	0.96094   0.96086   0.96078   0.96070   0.96062   0.96054   0.96046   0.9604	0.29348 0.29376 0.29404 0.29432 0.29460 0.29487	0.93596 0.93588 0.93579 0.93571 0.93562	1 0.31012   1 0.31040   1 0.31068   1 0.31095	0.95070 0.95061 0.95052	0.32667 0.32694 0.32722 0.32749	0.94514 0.94504 0.94495	56   55   54
5   0.26 6   0.26 7   0.26 8   0.26 9   0.26 10   0.26 11   0.26 12   0.26	022   0 050   0 079   0 107   0 135   0 163   0 191   0 219   0 247   0 275   0	. 96555   1 . 96547   1 . 96540   1 . 96532   1 . 96517   1 . 96502   1 . 96502   1 . 96494   1	0.27704   0.27731   0.27759   0.27787   0.27815   0.27843   0.27871   0.27879   1	0.96086   0.96078   0.96070   0.96062   0.96054   0.96046   0.9604	0.29376 0.29404 0.29432 0.29460 0.29487	0.95588 0.95579 0.95571 0.95562	0.31040     0.31068     0.31095	0.95061 0.95052	0.32694   0.32722   0.32749	0.94504	1 55 1 54
7   0.26 8   0.26 9   0.26 10   0.26 11   0.26 12   0.26	079   0 107   0 135   0 163   0 191   0 219   0 247   0 275   0 303   0	.96540   .96532   .96524   .96517   .96509   .96502   .96494	0.27759 i 0.27787 i 0.27815 i 0.27843 i 0.27871 i 0.27899 i	0.96070   0.96062   0.96054   0.96046	0.29432   0.29460   0.29487	0.95571 0.95562	0.31095		0.32749		
8   0.26 9   0.26 10   0.26 11   0.26 12   0.26	107   0 135   0 163   0 191   0 219   0 247   0 275   0 303   0	.96532   .96524   .96517   .96509   .96502   .96494	0.27787   0.27815   0.27843   0.27871   0.27899	0.96062   0.96054   0.96046	0.29460   0.29487	0.95562		0.95043		O GAARS	
9   0.26 10   0.26 11   0.26 12   0.26 13   0.26	135   0 163   0 191   0 219   0 247   0 275   0 303   0	.96524   .96517   .96509   .96502   .96494	0.27815   0.27843   0.27871   0.27879	0.96054 ! 0.96046 !	0.29487						
10   0.26 11   0.26 12   0.26 13   0.26	163   0 191   0 219   0 247   0 275   0 303   0	.96517   .96509   .96502   .96494	0.27843   0.27871   0.27899	0.96046		. ^ 05554					
11   0.26 12   0.26 13   0.26	191   0 219   0 247   0 275   0 303   0	.96509   .96502   .96494	0.27871 I 0.27899 I								
13 1 0.26	247   0 275   0 303   0	. 96494									
	275   0 303   0										
	202   0	. 46486	0.27927								
			0.27933								
			0.28011								
			0.28039								
			0.28067								
			0.28075   0.28123								
			0.28150								
22 1 0.26	500   0	.96425 I	0.28178 I	0.95948	0.29849	1 0.95441	1 0.31510	0.94906	0.33161	0.94342	1 28
			0.28206								
			0.28234								
			0.28242								
			0.28318								
			0.28346								
			0.28374 1								
			0.28402								
			0.28429								
			0.28457   0.28485								
			0.28513								
35   0.28	864 1 0	.96324 1	0.28541	0.95841	0.30209	0.95328	0.31848	0.94786	0.33518	0.94215	1 25
			0.28569								
			0.28597     0.28625								
			0.28652								
40 1 0.27	004   0	.96285	0.28680	0.95799	0.30348	0.95284	1 0.32006	0.94740	0.33655	0.94167	1 20
41   0.27	032   0	.96277	0.28708	0.95791	0.30376	0.95275	1 0.32034	0.94730	0.33682	0.94157	1 19
42   0.2	060   0	96269	0.28736	0.95782	0.30403	0.95266	0.32061	0.94721	0.33710	0.94147	1 18
			0.28764     0.28792								
45 1 0.2	144 1 0	.96246	0.28820	0.95757	1 0.30486	1 0.95240	1 0.32144	0.94693	1 0.33792	0.94118	1 15
46 1 0.2	172   0	.96238	0.28847	0.95749	0.30514	0.95231	1 0.32171	0.94684	0.33819	0.94108	1 14
			0.28875								
			0.28903     0.28931								
			0.28757								
			0.28987								
52 1 0.2	7340 1 0	.96190	0.29015	0.95698	1 0.30680	1 0.95177	0.32337	0.94627	0.33983	1 0.94049	1 8
			1 0.29042								
55 1 0.2	7424 1 0	). 701/4   ). 96166	0.29070     0.29098	1 0.75681 1 0 95677	1 0.30/36	1 0.75157	1 0.32392	1 0.74609	1 0.34038	1 0.94029	1 6
			1 0.29126								
57 1 0.2	7480 I 0	.96150	1 0.29154	0.95656	1 0.30819	1 0.95133	1 0.32474	0.94580	0.34120	1 0.93999	1 3
58 1 0.2	750B I 0	.96142	1 0.29182	1 0.95647	1 0.30846	1 0.95124	1 0.32502	1 0.94571	1 0.34147	1 0.93989	1 2
			0.29209								
			0.29237					· 0.94552	0.34202	1 0.93969 	
		SIN	cos	SIN	cos	SIN	cos	SIN	cos	SIN	- M
	74.		フヨ	5-	7=	2*	フ:	L <b>-</b>	70	>-	7

Table AII-1.—Natural Sines and Cosines—Continued

<del>-</del> -	20	•	21		22	-	23	•	24	•	
7	SIN	cos	SIN	cos	SIN	cos	SIN	cos	SIN	cos	
<u> </u>	0.34202 1	0.93969 1	0.35837 1	0.93358	0.37461 1	0.92718	0.39073	0.92050	0.40674 1	0.91355 1	60
1 1	0.34229 1	0.93959	0.35864 1	0.93348	0.37488 !	0.92707	1 0.39100 I	0.92039	0.40700	0.91343	59
2 1	0.34257	0.93949 1	0.35891 1	0.93337	0.37515	0.92697	I 0.39127 I	0.92028	0.40727	0.91331 (	58
3 1	0.34284	0.93939	0.35918	0.93327	0.37542	0.92686	1 0.39153 1	0.92016	0.40753	0.91319 (	57
4 1	0.34311	0.93929	0.35945	0.93316	0.37569	0.92675	0.37180	0.92005	0.40780 1	0.91307	56
5 I	0.34339 1	0.93919	0.35973	0.93306	0.37595     0.37622	0.92664	0.39207	0.91994	0.40806	0.71275	33
6 !	0.34366	0.93909 1	0.36000 1	0.93295	0.37622     0.37649	0.72633	1 0.37234 1	0.71782	0.40860	0.71203	53
- 1	0.34373	0.73877 1	0.36027 1	0.73283	0.37676	0.92631	0.39287	0.91959	0.40884	0.91260	52
9 1	0.34448	0.93879	0.36081	0.93264	0.37703	0.92620	0.39314	0.91948	0.40913	0.91248	51
10 1	0.34475	0.93849	0.36108	0.93253	0.37730	0.92609	0.39341	0.91936	0.40939	0.91236	50
11 1	0.34503	0.93859	0.36135	0.93243	1 0.37757 1	0.92598	1 0.39367 1	0.91925	0.40966	0.91224	1 49
12 1	0.34530	0.93849 1	0.36162	0.93232	1 0.37784 1	0.92587	1 0.39394 1	0.91914	1 0.40992 1	0.91212	1 48
13 1	0.34557	0.93839	0.36190 1	0.93222	1 0.37811 1	0.92576	0.39421	0.91902	0.41019	0.91200	47
14	0.34584	0.93829	0.36217	0.93211	0.37838	0.92565	1 0.39448	0.91891	0.41045	0.91188	46
15	0.34612	0.73817	0.36244	0.93201	0.37865	0.92554	1 0.374/4	0.718/7	0.410/2	0.711/6	1 44
					0.37892     0.37919						
					0.37746						
19	0.34721	0.93779	0.36352	0.93159	1 0.37973	0.92510	0.39581	0.91833	0.41178	0.91128	1 41
20	0.34748	0.93749	0.36379	0.93148	1 0.37999	0.92499	0.39608	0.91822	0.41204	0.91116	l, 40
					0.38026						
22	0.34803	0.9374B	0.36434	0.93127	1 0.38053	0.92477	1 0.39661	1 0.91799	1 0.41257	0.91092	
					0.38080						
					1 0.38107						
					1 0.38134						
26	0.34912	1 0.93708	0.36542	0.93084	0.38161	0.92432	1 0.39768	0.91752	0.41363	0.91044	1 34
27	0.34939	0.93698	0.36569	0.93074	0.38188	0.92421	1 0.39795	0.91741	0.41390	0.91032	1 22
28	0.34966	0.93688	0.36576	0.93063	1 0.38215	0.92410	1 0.37822	1 0.71727	1 0.41416	1 0.71020	1 34
27 70	0.34773	1 0.736//	1 0.36623	0.93052	0.38248	1 0.72377	1 0.37676	1 0.71716	1 0.41449	0.90996	1 30
31	0.35048	1 0.73667	1 0.36630	0.73072	0.38295	0.92377	1 0.37973	1 0.91694	1 0.41496	0.90984	1 29
32	0.35075	1 0.93647	0.36704	0.93020	0.38322	0.92366	0.39928	0.91683	1 0.41522	0.90972	1 28
33	0.35102	0.93637	1 0.36731	0.93010	0.38349	0.92355	0.39955	0.91671	1 0.41549	0.90960	1 27
34	0.35130	1 0.93626	0.36758	0.92999	1 0.38376	0.92343	1 0.39982	1 0.91660	1 0.41575	1 0.90948	1 26
35	0.35157	1 0.93616	0.36785	0.92988	1 0.38403	0.92332	1 0.4000B	0.91648	0.41602	0.90936	1 25
36	0.35184	1 0.93606	0.36812	0.92978	1 0.38430	0.92321	0.40035	0.91636	1 0.41628	1 0.90924	1 24
37	0.35211	1 0.93596	0.36839	0.92967	1 0.3B456	0.92310	0.40062	0.91625	0.41655	0.90911	1 20
					0.38483						
					0.38537						
					0.38564						
					1 0.38591						
43	0.35375	1 0.93534	1 0.37002	0.92902	0.38617	0.92243	1 0.40221	1 0.91555	1 0.41813	1 0.90839	1 17
					1 0.38644						
					0.38671						
					1 0.38698						
					0.38725 0.38752						
					1 0.38778						
					1 0.38805						
51	1 0.35592	0.93452	0.37218	1 0.92816	0.38832	1 0.92152	1 0.40434	1 0.91461	1 0.42024	1 0.90741	1 9
					0.38859						
53	1 0.35647	0.93431	1 0.37272	1 0.92794	1 0.38886	1 0.92130	1 0.40488	1 0.91437	1 0.42077	1 0.90717	1 7
54	1 0.35674	1 0.93420	1 0.37299	1 0.92784	1 0.38912	1 0.92119	1 0.40514	1 0.91425	1 0.42104	1 0.90704	1 6
55					1 0.38939						1 5
					1 0.38966						
					1 0.38993						
					1 0.37020						
					1 0.39073						
	cos	SIN	cos		cos		cos				
		~	 60						 :		– r
	-	•		_	<b>.</b>	-	٠.	_	<b>—</b>	_	

**Table AII-1.—Natural Sines and Cosines—Continued** 

M	25		26		27	-	28		29		
н Z	SIN	cos	SIN	cos	SIN	cos	SIN	cos	SIN	cos	
0 1	0.42262 1	0.90631	0.43837	0.89879	0.45399	0.89101	0.46947	0.88295	0.48481	0.87462	60
			0.43863 1								59
2 !	0.42315	0.90606	0.43889	0.89854	0.45451	0.89074	0.46999	0.88267	0.48532	0.87434	. 58
			0.43916 1								
			0.43942     0.43968								
			0.43788								
			0.44020								
			0.44046								
			0.44072								
			0.44098								
11	0.42552	0.90495	0.44124	0.89739	0.45684	0.88955	0.47229	0.88144	1 0.48761	1 0.87306	1 49
			0.44151								1 4B
			0.44177								1 47
			0.44203								
			0.44229								1 45
			0.44255     0.44281								
			0.44507								
			0.44333								
			0.44359								
			0.44385								
			0.44411								
			1 0.44437								
			1 0.44464								
			1 0.44490								
			0.44516								
28			1 0.44542								
			1 0.44568 1 0.44594								
30			1 0.44620								
			1 0.44646								
			1 0.44672								
33	0.43130	0.90221	1 0.44698	0.89454	1 0.46252	0.88661	1 0.47793	1 0.87840	0.49318	1 0.86993	1 27
			1 0.44724								
			1 0.44750								
			1 0.44776								
			0.44802 0.44828								
			0.44854								
			0.44880								1 20
			0.44906								1 19
			0.44932								
43			0.44958								1 17
44			0.44984								1 16
			1 0.45010								
			1 0.45036								
			1 0.45062								
			1 0.45088 1 0.45114								1 12
			1 0.45140								1 10
			1 0.45166								1 9
			0.45192								. , . 8
50	1 0.43654	1 0.89968	0.45218	1 0.89193	1 0.46767	1 0.88390	0.48303	0.87561	1 0.49824	1 0.86704	1 7
54	1 0.43680	1 0.89956	1 0.45243	0.89180	1 0.46793	0.88377	1 0.48328	1 0.87546	1 0.49849	1 0.86690	1 6
55	1 0.43706	1 0.89943	1 0.45269	L 0.89167	1 0.46819	1 0.88363	1 0.48354	0.87532	1 0.49874	1 0.86675	1 5
56	1 0.43733	0.89930	1 0.45295	0.89153	1 0.46844	0.88349	0.48379	1 0.87518	1 0.49899	0.86661	1 4
37	0.43759	0.87918	1 0.45321	0.89140	1 0.46870	0.88226	1 0.48405	0.87504	1 0.49924	0.86646	1 3
58	1 0.43785	1 0.89905	1 0.45347	0.89127	1 0.46896	0.88322	0.48430	1 0.87490	0.49950	0.86632	1 2
60	1 0.43837	1 0.89879	0.45373	1 0.89101	1 0.46947	1 0.88295	1 0.48421	1 0.874/5	1 0.499/5	0.86617	1 1
		SIN			cos	SIN		SIN	cos	SIN	- M
1	ھ ع	<b>1 -</b>	63	5-	64	2-	6	1 -	60	> <b>-</b>	7

**Table AII-1.—Natural Sines and Cosines—Continued** 

<u>-</u>	30		31	-	32	-	33	-	34	-	
7	SIN	cos	SIN	cos	SIN	cos	SIN	cos	SIN	cos	
0 1	0.50000 1	0.86603 1	0.51504	0.85717	0.52992	0.84805	0.54464	0.83867	0.55919	0.82904	60
1 1	0.50025	0.84588 I	0.51529	0.85702	0.53017	0.84789	0.54488	0.83851	0.55943	0.82887	59
2 !	0.50050 1	0.84573	0.51554	0.85687	0.53041   0.53066	0.84774	0.34313	0.83835	0.33768     0.33992	0.82871 1	38
<b>3</b> :	0.50078 1	0.86537 I	0.51574 1	0.85457	0.53091	0.84743	0.54561	0.83804	0.56016 1	0.82839	56
					0.53115						55
6 1	0.50151	0.86515 i	0.51453	0.85427	0.53140 I	0.84712	0.54610	0.83772	0.56064	0.82804	54
7 !	0.50176 1	0.86501	0.51678	0.85412	0.53164	0.84697	0.54635	0.83756	0.54088	0.82790	53
					0.53199     0.53214						
					0.53238						
11 1	0.50277	0.86442	0.51778	0.85551	0.53263	0.84635	0.54732	0.83492	I 0.56184 I	0.82724 I	1 49
					0.53288 1						
					0.53312						
					0.53337     0.53341						40   45
					0.53384						
17 1	0.5042B	0.86354	0.51927	0.85461	0.53411	0.84542	0.54878	0.83597	0.56329	0.82626	1 43
					1 0.53435						
					0.53460     0.53484						
					0.53509						
22	0.50553	0.84281	0.52051	0.85385	1 0.53534 1	0.84464	1 0.54999	0.83517	1 0.56449	0.82544 I	
					0.53558						
					1 0.53583   1 0.53607						
					0.53632						
					1 0.53656						
28	0.50704	0.86192	0.52200	0.85294	1 0.53681	0.84370	0.55145	0.83421	0.54593	0.82446	ı 32
					0.53705						
					0.53730						
					1 0.53754   1 0.53779						
					0.53804						
					0.53828						
					1 0.53853						
					0.53877						
					0.53902						
					0.53951						
40	0.51004	0.86015	0.52498	0.85112	1 0.53975	0.84182	1 0.55436	1 0.83228	1 0.56880	0.82248	1 20
					1 0.54000						
					1 0.54024						
					1 0.54073						
45	0.51129	0.85941	0.52621	0.85035	1 0.54097	0.84104	1 0.55557	1 0.83147	1 0.57000	0.82165	1 1:
					1 0.54122						
					1 0.54146						
					1 0.54195						
50	0.51254	0.85844	0.52745	1 0.84959	1 0.54220	0.84025	1 0.55678	1 0.83066	1 0.57119	0.82082	1 1
					1 0.54244						
					1 0.54269						
					1 0.54317						
55	0.51379	0.85792	0.52849	1 0.84882	1 0.54342	1 0.83946	1 0.55799	1 0.82985	1 0.57238	1 0.81999	1
					0.54366						
					1· 0.54391 1 0.54415						
					0.54440						
					1 0.54464						
	cos		cos		cos					SIN	
	59		 58		 57				s		-

**Table AII-1.—Natural Sines and Cosines—Continued** 

1	35	•	36	.•	37	•	38	•	39	•	
1	SIN	cos	SIN	cos	SIN	cos	SIN	cos	SIN	cos	-
			0.58779								
1 1	0.57381 1	0.81899	0.58802	0.80885	0.60205	0.79846	0.61589	0.78783	0.42955	0.77494	1 59
			0.58824								
			0.58849								
			0.58873     0.58896								
			0.58920								
			0.58943								
1	0.57548	0.81782	0.58967	0.80765	0.60367	0.79723	1 0.61749	0.78658	0.63113	0.77548	1 5
. 1	0.57572	0.81765	0.58990	0.80748	0.60390	0.79706	0.61772	0.78640	0.43135	1 0.77550	1 5
' !	0.57596	0.81748	0.59014	0.80730	0.60414	0.79688	0.61795	0.78622	0.63158	0.77531	1 5
. !	0.57619	0.81731	0.59037	0.80713	0.60437	0.79671	0.61818	0.78604	0.63180	0.77513	! 4
			0.59061   0.59084								
	0.57491	0.81481	0.57108	0.80677	0.60465	0.77633	1 0.01007	0.78568	0.63225	0.77476	
	0.57715	0.81664	0.57131	0.80644	0.60508	0.79400	1 0.61887	0.78550	1 0.63278	1 0.77438	1 4
, ,	0.57738	0.81647	0.59154	0.80627	0.60553	0.79583	1 0.61932	0.78514	0.63271	1 0.77431	1.7
' 1	0.57762	0.81631	0.59178	0.80610	0.60576	0.79565	0.61955	0.78496	0.63316	1 0.77402	i 4
1	0.57786	0.81614	0.59201	0.80593	0.60599	0.79547	0.61978	0.78478	0.63338	0.77384	i 4
' 1	0.57810	0.81597	0.59225	0.80576	0.60622	0.79530	1 0.62001	0.78460	0.63361	1 0.77366	1 4
)	0.57833	0.81580	0.59248	0.80558	0.60645	0.79512	0.62024	0.78442	0.63383	0.77347	1.4
. 1	0.57857	0.81563	0.59272	0.80541	0.60668	0.79494	0.62046	0.78424	0.63406	1 0.77329	1 3
!!	0.57881	0.81546	0.59295	0.80524	0.60691	0.79477	0.62069	0.78405	0.63428	1 0.77310	1 3
	0.57904	0.81530	0.59318	0.80507	0.60714	0.79459	0.62092	0.78387	0.63451	0.77292	1 3
. !	0.57928	0.81513	0.59342	0.80489	0.60738	0.79441	0.62115	0.78369	0.63473	0.77273	1 3
	0.37934	0.81476	0.59365	0.804/2	0.60761	0.79424	0.62138	0.78351	0.63496	1 0.77255	! :
. ;	0.57999	0.81442	0.59389     0.59412	0.80433	1 0.60784	0.77406	0.62160	0.78333	0.63518	0.77236	! ;
ı	0.58023	0.81445	0.59436	0.80420	0.808.0	1 0.77366	1 0.62163	1 0.78313	1 0.63340	0.77218	! :
,	0.58047	0.81428	0.59459	0.80403	0.60853	1 0.79353	1 0.62229	1 0.78279	1 0.83383	1 0.77191	; ;
) 1	0. <b>580</b> 70	0.81412	1 0.59482	0.80386	1 0.60B76	0.79335	1 0.42251	I 0.78261	L O. ASAOR	1 0.77162	1 '
ιı	0.58094	I 0.81395	0.59506	0.80368	0.60899	0.79318	1 0.62274	1 0.78243	0.63630	1 0.77144	1 :
: 1	0.58118	0.81378	0.59529	0.80351	0.60922	0.79300	1 0.62297	1 0.78225	7747A.O. I	1 0.77125	1 :
,	0.58141	0.81361	∤ 0.59552 ∣	0.80334	1 0.60945	1 0.79282	1 0.62320	1 0.7820A	1 0.43475	1 0.77107	1 2
	0.38165	0.81344	0.59576	0.80316	0.6096B	0.79264	0.62342	0.78188	0.63698	1 0.77088	1 2
,	0.38187	0.81227	0.59599	0.80299	0.60991	1 0.79247	0.62365	0.78170	0.63720	0.77070	1 2
	0.58236	0.81310	0.59622	0.80282	0.61015	0.79229	0.62388	0.78152	0.63742	0.77051	1 3
	0.58260	0.81276	0.57669	0.80284	1 0.61038	1 0.79211	0.62411	0.78134	0.63765	0.77033	! :
,	0.58283	0.81259	0.59693	0.80230	0.61084	1 0.77175	1 0.62455	1 0.78118	1 0.63/8/	1 0.77014	: :
•	0.38307	0.81242	1 0.59716	1 0.80212	0.61107	1 0.79158	1 0.62479	1 0.78079	1 O. A3832	1 0.74977	. :
	0.58330	0.81225	1 0.59739	0.80195	1 0.61130	1 0.79140	1 0.62502	0.78061	L 0. 63854	1 0 74959	
2	0.58354	1 0.81208	1 0.59763	1 0.80178	1 0.61153	1 0.79122	1 0.62524	1 0.78043	1 0 43877	1 0 74940	
	0.58378	1 0.81191	1 0.59786	0.80160	0.61176	1 0.79105	1 0.62547	1 0.78025	1 0. ATR99	1 0 74921	
•	0.58401	0.81174	1 0.59809	1 0.80143	1 0.61199	1 0.79087	1 0.62570	1 0.78007	1 0.43922	1 0 74903	
	0.58445	0.81157	0.59832 0.59856	0.80125	0.61222	1 0.79069	0.62592	0.77988	0.63944	1 0.76884	1
,	0.58472	1 0.81123	0.59879	1 0.80108	1 0.01245	1 0.79051	0.62615	1 0.77970	1 0.63966	1 0.76866	1
,	0.38496	1 0.B1106	1 0.59902	1 0.80073	1 0.61291	1 0.79016	1 0.62660	1 0.77934	1.0.64011	1 0 74929	
,	0.58519	0.81089	1 0.59926	0.80056	0.61314	1 0.78998	1 0.62683	1 0.77916	7.7.0AA.O. I	L 0 74810	
,	0.58543	0.81072	1 0.59949	1 0.80038	1 0.61337	1 0.78980	1 0.62706	I 0.77897	1 0 64054	1 0 74791	
1	0.58567	1 0.81055	1 0.59972	1 0.80021	1 0.61360	1 0.78962	1 0.6272B	I 0.77879	1 0 64078	1 0 74777	1
2	0.58590	1 0.81038	0.59995	1 0.80003	1 0.61393	1 0.78944	1 0.42751	1 0 77841	1 0 44100	1 0 74784	
5	0.58614	1 0.81021	1 0.60019	1 0.79986	1 0.61406	1 0.78924	1 0 62774	I 0 77843	I A 44123	1 0 74775	
4	0.58637	1 0.81004	1 0.40042	1 0.79948	1 0 61420	1 0 70000	1 0 42784				
•	0.58661	0.80987	1 0.60065	1.0.79951	1 0.61451	1 0.78891	1 0.62819	1 0.77806	L 0.64167	1 0 74498	1
3	0.58684	1 0.809/0	1 0.60089	1 0.79934	1 0.61474	1 0.78873	1 0.62842	1 0.77788	1 0 64190	1 0 74470	
•	1 0.58708	1 0.80733	0.60112	1 0.79916	0.61497	0.78855	1 0.62864	0.77769	0.64212	1 0.76661	!
7	1 0.58755	0.80738	0.60135	1 0.79899	0.61520	1 0.78837	1 0.62887	0.77751	0.64234	0.76642	!
0	0.58779	0.80902	0.60182	0.79864	1 0.61564	0.78801	1 0.62939	1 0.77733	0.64256	1 0.76623	!
	cos	SIN	cos	SIN							
	_====				cos		cos	SIN.	cos	SIN	
	5/	ı <b>-</b>	53	ς •	52	<b>-</b>	<b>5</b> .		50		

**Table AII-1.—Natural Sines and Cosines—Continued** 

<u> </u>	40		41		42		43		44		
7	SIN		SIN	cos	SIN	cos	SIN	cos	SIN	C0 <b>\$</b>	•
					0.66913 1						
					0.66935						
					0.66956   0.66978						
					0.66999						
					0.67021						
					0.67043 1						
					0.67064						
					0.67086 1						
					0.67107						
					0.67151						
					0.67172						
					0.67194						
					0.67215						
					0.67237     0.67258						
					0.67280						
					0.67301						
					0.67 <b>32</b> 3						
					0.67344						
					0.67366     0.67 <b>38</b> 7						
					0.67409						
					0.67430						
					0.67452						
					0.67473						
					0.67495						
					0.67516     0.67538						
					1 0.67559						
					0.67580						
					1 0.67602						
33 1	0.65011	1 0.75984 1	0.66327	0.74838	1 0.67623	0.73669	1 0.48879	0.72477	0.70153	0.71264	1 27
					1 0.67645						
					0.67666						
					1 0.67688 1 0.67709						
					1 0.67730						
					0.67752						
40	0.45166	0.75851	0.66480	1 0.74703	1 0.67773	0.73531	1 0.69046	0.72337	1 0.70298	0.71121	1 20
					0.67795						
					0.67816 0.67837						
					1 0.67859						
					1 0.67880						
					1 0.67901						
					0.67923						
					1 0.67944						
					1 0.67965						
					1 0.68008						
					1 0.68029						
53	0.65452	1 0.75604	1 0.66762	1 0.74451	1 0.68051	1 0.73274	1 0.69319	1 0.72075	1 0.70567	1 0.70855	1 7
					1 0.68072						
					0.68093 0.68115						
					1 0.68136						
					0.68157						
59	1 0.65584	1 0.75490	1 0.66891	1 0.74334	1 0.68179	1 0.73155	1 0.69445	1 0.71954	1 0.70690	1 0.70731	1 1
					1 0.68200						
	cos	SIN	cos	SIN	cos	SIN	cos	SIN	cos	SIN	
	49		 48		47		4		4:		- :
		<u>-</u>		<del>-</del>						_	•

Table AII-2.—Natural Tangents and Cotangents

M			1-		2	•	3	•	4	-	- 1
н <b>2</b>	TAN	COT	TAN	COT	TAN	COT	TAN	COT	TAN	COT	.
0 1	0000000 1 0	0000000 1	0.01746	57.2900 I	0.03492	28.6363 1	0.05241 1	17.0811	0.06993 1	14.3007	60
1 I	0.00029	3437.75	0.01775	56.3506	0.03521	28.3994	0.05270	18.9755	0.07022 1	14.2411	59 58
2 !			0.01833 I						0.07080		36   57
3	0.00087	1173.72   RSQ.434	0.01862 I	53.7086 I	0.03409 1	27.7117	0.05357	18.6654			56
5 i	0.00145	687.549 1	0.01871 I	52.8821	0.03638	27.4899	0.05387	18.5445 I	0.07139	14.0079	155
6 1	0.00175   3	572.957 I	0.01920 I	52.0807	0.03667	27.2715	0.05416 1	18.4645	0.07168	13.9507	54
7 1	0.00204	491.106 1	0.01949	51.3032	0.03696	27.0566	0.05445	18.3455	0.07197	13.8940	53
8 !	0.00233	429.718	0.01978 !	50.5485	0.03725	26.8450	0.05474	18.2677	0.07227	13.8378	1 52
9 I 10 I	0.00262	381.9/1	0.02007   0.02036	47.813/	0.03/34	26.8367	0.05533	18.0750	0.07285	13.7247	50
111	0.00271   3	312.521	0.02066 1	48.4121	0.03812 1	26.2296	0.05562 J	17.9802	0.07314 1	13.6719	49
12			0.02095								1 48
13 1	0.00378	264.441	0.02124	47.0853 I	0.03871 1	25.8348	0.05620	17.7934	0.07373 1	13.5634	1 47
14	0.00407 1		0.02153								1 46
15			0.02182								1 45
16			0.02211								! 44
17			0.02240								1 42
18			0.02289								41
20			0.02328								1 40
21 1			0.02357								
22 1			0.02386								1 28
23 1			0.02415						1 0.07665 1		
24 1			0.02444 1						1 0.07695		
25			0.02473						1 0.07724		
26 !			0.02502						1 0.07753   1 0.07782		1 34
27 !			0.02531   0.02560				0.06029     0.06058				
29			0.02589						0.07841		i 31
			0.02619						0.07870		
31 1	0.00902 1	110.892	0.02648	37.7686	1 0.04395	22.7519	1 0.06145	16.2722		12.6591	
	0.00931	107.426	0.02677	37.3579	0.04424	22.6020	1 0.06175	16.1952	0.07929		1 28
22			0.02706								
34			0.02735						0.07987     0.08017		1 26
35			0.02793						1 0.08046		24
	0.01076	92.9085	0.02822	35.4313	0.04570	21.8813	0.06321	15.8211			1 23
28 I	0.01105	90.4633 1	0.02851	35.0695	1 0.04599	21.7426	0.06350	15.7483			1 22
39 1			0.02881								1 21
40 1			0.02910								1 20
41			0.02939   0.02968								1 19
43			1 0.02987 1								1 17
44			0.03026							1 12.0772	
			0.03055							1 12.0346	1 15
46 1	0.01338	74.7292	1 0.03084 1	32.4213	0.04833	1 20.6932	1 0.06584	15.1893		1 11.9923	
			1 0.03114 1							1 11.9504	1 13
			0.03143 1								1 12
			1 0.03172     0.03201								11
			1 0.03201 1								1 10
			1 0.03250 1								
			1 0.03288 1								
			1 0.03317 1								
55	1 0.01600 I	62.4992	1 0.03346 1	29.8823	1 0.05095	1 19.6273	1 0.06847	1 14.6059	1 0.08602	1 11.6248	1 5
			1 0.03376 1								
			1 0.03405 [								
			1 0.03434 I 1 0.03463 I								
			1 0.03483 1								
	COT	TAN	COT	TAN	COT	TAN	COT	TAN	COT	TAN	
											– ː
1	89 		88			, . 		> - 		 	

**Table AII-2.—Natural Tangents and Cotangents—Continued** 

				<del></del>	···········					<del></del>	
<u>~</u> _	5-								9		
Ĭ N	TAN C	OT	TAN	COT	TAN	COT	TAN	COT	TAN	COT	•
0 1	0.08749   11	.4301 1	0.10510	9.51436	0.12278 !	8. 14435	0.14054	7.11537	0.15838	6.31375	60
	0.08778   11										
	0.08807   11										
3 1	0.08837   11	.3165	0.10599	9.43515	0.12367	8.08600	0.14143	7.07059	0.15928	6.27829	57
3	0.08866   11	2417 1	0.10628 1	9.40904	1 0.12397 1	8.066/4	0.141/3	7.055/9	0.15938	6.26633	26
	0.08925   11										
7 1	0.08954   11	. 1681	0.10716	9.33155	1 0.12485 1	8.00948	1 0 14242 1	7.02037	1 0 16047	4 23140 H	53
	0.08983   11										
	0.09013   11										
	0.09042   11										
	0.09071   11										
12	0.09101   10	. 9882	0.10863	9.20516	0.12622	7.91582	1 0.14410	6.93952	1 0.16196	6.17419	48
13	0.09130   10	. 9529	0.10893	9.18028	0.12662	7.89734	1 0.14440 1	6.92525	0.16226	6.16283	47
14 1	0.09159   10	9.71/8 1	0.10922	9.15554	0.12692	7.87895	1 0.14470 1	6.91104	0.16256	6.15151	46
15	0.09189   10	0.8827	0.10952	9.13093	0.12722	7.86064	1 0.14499	6.89688	0.16286	6.14023	45
17	0.09218   10   0.09247   10	1.0403 I	0.10781	9.10546	1 0.12/51	7.84242	0.14529	6.98278	0.16316	6.12879	44
18	0.09277   10	7797 1	0.11040	9.05789	1 0.12/81	7.04720	1 0.14337	0.005/7 1 05475	0.16346	6.11//9	43
19	0.09306   10	.7457	0.11070	9.03379	1 0.12840	7.00022	1 0.1451B	6.83473	1 0.16376	1 6.10 <del>007</del>	42
20 1	0.09335   10	.7119	0.11099	9.00983	0.12869	7.77035	1 0.1464B	A. 82494	1 0.16435	6.07332	40
21	0.09365   10	.6783	0.11128	8.98598	0.12899	7.75254	1 0.14678	6.81312	1 0.16465	6.07340	1 39
22 1	0.09394   10	.6450 I	0.11158	8.96227	0.12929	7.73480	1 0.14707	6.79936	1 0.16495	6-06240	1 38
23	0.09423   10	.6118	0.11187	8.93867	0.12958	7.71715	1 0, 14737	6.78564	1 0.14525	L A. 05143	1 37
24	0.09453   10	).5789 I	0.11217	8.91520	0.12988	7.69957	1 0.14767	6.77199	I 0.14555	I A. 04051	AZ I
25	! 0.09482   10	.5462	0.11246	8.89185	0.13017	7.68208	1 0.14796	6.75838	1 0.14585	6.02962	1 35
26	0.09511   10	.5136	0.11276	8.86862	1 0.13047	7.66466	1 0.14826	6.74483	1 0.16615	6.01878	34
27	0.09541   10	.4813	0.11305	8.84551	1 0.13076	7.64732	0.14856	6.73133	0.16645	6.00797	ı 33
28	0.09570   10	.4491	0.11335	8.82252	0.13106	7.63005	0.14886	6.71789	1 0.16674	5.99720	1 32
29	0.09600   10	7.4172	0.11364	8.79964	0.13136	7.61287	1 0.14915	6.70450	0.16704	5.98646	1 31
30	0.09629   10	. 3834	0.11394	9.77689	0.13165	7.59575	0.14945	6.69116	0.16734	5.97576	1 30
37	0.09658   10   0.09688   10	7.3338	0.11423	8.75425	0.13195	7.57872	0.14975	6.67787	0.16764	5.96510	1 27
22	0.09717   10	2017	0.11432	0.73172	1 0.13224	7.301/6	0.15005	0.00403	0.16794	5.93448	28
34	0.09746   10	2602	0.11511	B. 68701	1 0.13234	1 7.3770/	1 0.15054	1 0.03144	0.16824	1 5.74370	1 2/
35	0.09776   10	. 2294	0.11541	8.66482	1 0.13313	7.51132	1 0.15084	1 6.65651	1 0 14004	1 5.73333	1 25
36	0.09805   10	. 1988	0.11570	8.64275	1 0.13343	7.49465	1 0. 15124	1 6.61219	1 0. 16914	1 5.9123A	1 23
37	0.09834   10	).1683	0.11600	8.62078	1 0.13372	1 7.47806	1 0.15153	1 6.59921	1 0.16944	1 5.90191	1 23
2B	0.09864   10	).1381	0.11629	8.59893	1 0.13402	7.46154	1 0.15183	L A. 58A27	1 0.14974	5 89151	1 22
39	0.09893   10	).10B0	0.11659	8.57718	0.13432	7.44509	1 0.15213	6.57339	L 0.17004	1 5.88114	1 21
40	0.09923   10	).07B0	I O.11688	I 8.55555	1 0.13461	1 7.42871	1 0.15243	L A. 5A055	1 0.17033	1 5 87080	1 20
41	0.09952   10	0.04B3	0.11718	8.53402	0.13491	7.41240	1 0.15272	1 6.54777	0.17063	5.86051	1 19
42	0.09981   10	0.0187	0.11747	8.51259	0.13521	7.39616	1 0.15302	6.53503	1 0.17093	1 5.85024	1 18
144	0.10011   9.	94907	0.11777	8.49128	0.13550	7.37999	0.15332	6.52234	0.17123	5.84001	1 17
45	0.10040   9.   0.10069   9.	93101	1 0.11806	8.4/007	0.13580	1 7.36389	0.15362	6.50970	0.17153	5.82982	1 16
46	0.10097   7.	90211	0.11865	B. 42795	1 0.13607	1 /.34/86	1 0.15371	1 6.49/10	0.17183	3.81766	15
47	0.10128   9.	87338	0.11895	B. 40705	1 0.13669	1 7.31400	1 0.15451	1 A 47204	1 0.1/213	1 5 70044	1 17
48	! 0.'10158   9.	. 84482	1 0.11924	1 8.38625	1 0.13698	1 7.30018	1 0.15481	I A. 459A1	1 0.17273	1 5 79939	1 12
49	0.10187   9.	81641	0.11954	8.36555	1 0.13728	1 7.28442	1 0.15511	I A. 44720	1.0.17303	1 5 77934	
30	1 0.10216 1 9.	. 788 17	0.11983	I 8.34496	1 0.13758	7.26873	1 0.15540	I A. ATARA	1 0 17333	1 5 74937	1 10
[51	0.10246   9.	. 76009	1 0.12013	1 8.32446	I 0.13787	7.25310	L 0.15570	I A. 42253	1 0 17363	1 5 75941	
1 52	1 0.10275 1 9.	. 73217	1 0.12042	B. 3040A	1 0.13817	1 7 23754	1 0 15400	1 4 41024	1 0 17707	S 74846	
1 22	1 0.10305 1 9.	.70441	1 0.12072	1 8.28376	I 0.13B46	1 7.22204	1 0.15630	1 4.39804	1 0.17423	1 5 73940	. 7
34	1 0.10334 1 9.	. 67680	0.12101	1 8.26355	1 0.13876	1 7.20661	1 0.15660	L A. 38587	1 0.17453	1 5 72974	1 4
22	1 0.10363 1 9.	. 64935	0.12131	1 8.24345	1 0.13906	1 7.19125	1 0.15689	I 6.37374	1 0.17483	1 7 71992	
57	0.10393   9.   0.10422   9.	59490	1 0.12160	1 0.22344	0.13935	1 7.17594	0.15719	6.36165	0.17513	5.71013	1 4
58	0.10452   9.	. 56791	1 0. 12219	1 B. 1937A	1 0 1700	1 7 14557	1 0.13/49	1 6.34961	0.17543	5.70037	1 3
59	0.10481   9.	54106	1 0.12249	8.14398	1 0.14024	1 7.13042	1 0.15779	1 6.33/61	1 0.1/3/3	1 5.07064	1 2
60	1 0.10510   9.	51436	0.12278	8.14435	0.14054	7.11537	0.15838	1 6.31375	1 0.17633	5.67128	1 0
		TAN		TAN		TAN		TAN		TAN	
											- ï
1_	84*		83	5 <b>-</b>	82	2 •	8 1	L <b>-</b>	80	>-	7
		<del></del>									

Table AII-2.—Natural Tangents and Cotangents—Continued

	10		11		12		13	-	14		
I											-
2	TAN	COT	TAN	COT	TAN	COT	TAN	COT	TAN	COT	
0	0.17633 1	5.67128	0.19438	5. 14455	0.21256	4.70463	0.23087	4.33148	0.24933	4.01078	1 60
	0.17663										
	0.17693     0.17723										
	0.17723     0.17753										
5	1 0.17783 I	5.62344 1	0.19 <b>58</b> 9 I	5. 10490	0.2140B I	4.67121	0.23240	4.30291	0.25087	3.98607	1 55
	0.17813										
	0.17843     0.17873										
	0.17903 I										
	0.17933										
	0.17963     0.17993										
	1 0.17773 I										
14	I 0.18053 I	5.53927	0.19861	5.03499	0.21682	4.61219	0.23516	4.25239	0.25366	3.94232	1 46
	0.18083										
	0.18113										
	0.18173										
	I 0.18203 I										
	0.18233										
	0.18263   0.18293										
	0.18323										
	1 0.18353 1										
1	0.18384										
	0.18414     0.18444										
	1 0.18474 1										
	I 0.18504 I										
	0.18534     0.18544										
1	1 0.18594 1										
	I 0.18624 I										
	1 0.18654 1										
	0.18684     0.18714										
	1 0.18745										
28	1 0.18775	5.32631	0.20588	4.85727	1 0.22414	1 4.46155	1 0.24254	1 4.12301	1 0.26110	1 3.82992	1 22
	1 0.18805										
	0.18835										
42	1 0.18895 1	5.29235	0.20709	4.82882	1 0.22536	1 4.43735	1 0.24377	1 4.10216	1 0.24235	1 3.81177	1 18
	1 0.18925 1										
	1 0.18955 I 1 0.18986 I										
	1 0.19016 1										
47	1 0.19046 I	5.25048	1 0.20841	1 4.79370	1 0.22689	1 4.40745	1 0.24532	1 4.07639	1 0.26390	1 3.78931	1 13
	1 0.19076 1										
	0.19106     0.19136										
51	1 0.19166 I	5.21744	0.20982	1 4.76595	0.22811	4.38381	1 0.24655	1 4.05599	0.26515	1 3.77152	1 9
	1 0.19197 1										
	0.19227     0.19257										
	1 0.19287 1										
56	I 0.19317 I	5.17671	1 0.21134	1 4.73170	1 0.22964	1 4.35459	1 0.24809	1 4.03076	1 0.26670	1 3.74950	1 4
	1 0.19347 1										
	1 0.19378 1										
	0.19438										
-	COT	TAN	COT	TAN	COT	TAN	COT	TAN	COT	TAN	 m
1	79		 76		 77						- I
1-				- 				- 	フ: 		
1											

Table AII-2.—Natural Tangents and Cotangents—Continued

7	15	-	16	-	ュア	-	18	-	19	-	
7	TAN	COT	TAN	COT	TAN	COT	TAN	COT	TAN	COT	-
0 1	0.26795	3.73205	0.28675	3.48741	0.30573	3.27085	0.32492	3.07768	0.34433	2.90421	1 60
									0.34465		
									0.34498		
									0.34530		57
									0.34563     0.34596		55
									0.34628		
									0.34661		
									0.34693		
									0.34726		
									0.34758		
									0.34791     0.34824		
									0.34856		
									0.34889		
									1 0.34922 1		
16 i	0.27294 1	3.66376	0.29179	3.42713	0.31083	3.21722	I 0.33007 I	3.02963	1 0.34954 1	2.86089	1 44
									1 0.34987 1		
									0.35020		
									0.35052		
									0.35085		
									0.35118     0.35150		1 39
									0.35183		
									0.35216		
									0.35248		1 3
									0.35281		
									1 0.35314		
									0.35346		
									0.35379		1 3
									0.35412     0.35445		
									0.35477		
									0.35510		
									0.35543		
32 1	0.27889	3.58562	1 0.29780	3.35800	0.31690	3.15558	1 0.33621	1 2.97430	1 0.35576	2.81091	1 2
									0.35608		
									0.35641		
									1 0.35674		
									1 0.35740		
									0.35772		
42	0.28109	3.55761	0.30001	3.33317	1 0.31914	3.13341	0.33848	1 2.95437	1 0.35805	1 2.79289	1 1
									0.35838		1 1
									0.35871		1 1
									1 0.35904		! 1
									1 0.35937		! 1
									1 0.35969		
									1 0.36035		
									1 0.36068		1 1
51	0.28391	3.52219	1 0.30287	1 3.30174	1 0.32203	1 3.10532	1 0.34146	1 2.72710	1 0.36101	1 2.77002	
52	0.28423	3.51829	0.30319	1 3.29829	0.32235	1 3.10223	1 0.34173	1 2.92632	1 0.34134	1 2.76750	1
									1 0.36167		
									1 0.36199		
56	0.28549	1 3.50279	1 0.30414	1 3.48/73	1 0.32331	1 3.07278	1 0.342/0	1 2.71/77	1 0.36232	1 2./3776	1
57	0.28580	3.49894	1 0.3047B	1 3.28109	1 0.32394	1 3.08485	1 0.34335	1 2.91244	1 0.36298	1 2.75494	i
58	0.28612	3.49509	1 0.30509	1 3.27767	1 0.32428	1 3.08379	1 0.34368	1 2.90971	1 0.36331	1 2.75246	1
59	1 0.28643	1 3.49125	1 0.30541	1 3.27426	1 0.32460	1 3.08073	1 0.34400	1 2.90696	1 0.36364	1 2.74997	1
60 	· 0.28675	3.48741 	1 0.30573	1 3.27085	1 0.32492	1 3.07768	1 0.34433	1 2.90421	1 0.36397	1 2.74748	1_
	COT	TAN	COT		COT				COT	TAN	
	フィ	<b></b>	<b>ブ</b> 3	5-	72		7:			<b>&gt;-</b>	
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Table AII-2.—Natural Tangents and Cotangents—Continued

Γ		····				
m	20.	21*		23*	24*	
7	TAN CO	T TAN C	OT TAN COT	TAN COT	TAN C	oT
	1 0.36397   2.747	48   0.38386   2.6	0509   0.40403   2.47509	1 0.42447 1 2.35585	1 0.44523 1 2.2	4604 1 60
			0283   0.40436   2.47302			
			0057   0.40470   2.47095			
			9831   0.40504   2.46888 9606   0.40538   2.46682			
			9381   0.40572   2.46476		1 0.44697 1 2.2	
			9156   0.40606   2.46270			
			8932   0.40640   2.46065			
			8708   0.40674   2.45860			
			8484   0.40707   <b>2.4565</b> 5 8261   0.40741   2.4 <b>5</b> 451			
			8038   0.40775   2.45246			
1			7815   0.40809   2.45043			
			7593   0.40843   2.44839			
14	1 0.36859 1 2.713	05   0.38854   2.5	7371   0.40877   2.446 <mark>3</mark> 6	1 0.42929 1 2.32943	1 0.45012 1 2.2	22164   46
			7150   0.40911   2.44433			
			6928   0.40945   2.44230			
			6707   0.40979   2.44027 6487   0.41013   2.43825			
			6266   0.41047   2.43623			
			6046   0.41081   2.43422			
			5827   0.41115   2.43220			
			5608   0.41149   2.43019 5389   0.41183   2.42819			
			5170   0.41217   2.42618			
			4952   0.41251   2.42416			
			4734   0.41285   2.42218			
			4516   0.41319   2.42019			
			4299   0.41353   2.41819			
			4082   0.4138 <u>7</u>   2.41620 3865   0.41421   2.4142			
			3648   0.41455   2.4122			
			3432   0.41490   2.4102:			
			3217   0.41524   2.40827			
			3001   0.41558   2.40629 2786   0.41592   2.40432			
			2571   0.41626   2.4023			
			2357   0.41660   2.40036			
			2142   0.41694   2 <b>.398</b> 4:			18084   22
			1929   0.41728   2.3964			17916   21
			61715   0.41763   2.3944° 61502   0.41797   2.3925			
			31289   0.41831   2.3905			
			1076   0.41865   2.3886			
44	1 0.37853   2.64	177   0.3 <mark>98</mark> 62   2.5	50864   0.41899   <b>2.38</b> 666	3   0.43966   2.27447	1 0.46065 1 2.	17083   16
			50652   0.41933   2.3847			
			50440   0.41968   2.3827 <sup>4</sup> 50229   0.42002   2.3808 <sup>4</sup>			
			50018   0.42036   2.3808			
			19807   0.42070   2.3769			
			19597   0.42105   2.3750			
			19386   0.42139   2.3731			
			19177   0.42173   2.37119 18967   0.42207   2.3692			
			18758   0.42242   2.3673			
55	I 0.38220 I 2.61	646   0.40234   2.4	18549   0.42276   2.3654	1   0.44349   2.25486	1 0.46454 1 2.	15268   5
			18340   0.42310   2.3634			
			18132   0.42345   2.3615 17924   0.42379   2.3596			
			17716   0.42413   2.3577			
			17509   0.42447   2.3558			
			AN COT TAN			
	69*			66*	 6 <b>5°</b>	I
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**Table AII-2.—Natural Tangents and Cotangents—Continued** 

<u> </u>		**************************************				
M	25-	26*	27•	28*	29*	
7	TAN CO	TAN COT	TAN COT	TAN COT	TAN COT	-
0	1 0.46631 1 2.1445	1   0.48773   2.05030	1 0.50953   1.96261	0.53171   1.88073	0.55431   1.80405	1 60
		8   0.48809   2.04879				
		5   0.48845   2.04728				
		3   0.48881   2.04577				
		1   0.48917   2.04426				
		39   0.48953   2.04276 77   0.48989   2.04125				
		6 1 0.49026 1 2.03975				
		64 1 0.49062 I 2.03825				
		3   0.49098   2.03675				
		2   0.49134   2.03526				
		1   0.49170   2.03376				
		1   0.49206   2.03227				
		50   0.49242   2.03078				
14	0.47128   2.1219	0   0.49278   2.02929	1 0.51467 1 1.94301	0.53694   1.86239	0.55964   1.78685	1 46
		0   0.49315   2.02780				
		1   0.49351   2.02631				
		11   0.49387   2.02483				
		52   0.49423   2.02335				
		72   0.49459   2.02187				
20	1 0.4/341   2.1123	33   0.49495   2.02039	0.51688   1.93470	0.53920   1.85462	0.56194   1.77955	1 40
22	1 0.4/3// 1 2.1107	75   0.49532   2.01891	0.51724   1.93332	0.53957   1.85333	0.56232   1.77834	1 39
27	1 0.47412 1 2.107	16   0.49568   2.01743	1 0.51761   1.93195	0.53995   1.85204	0.56270   1.77713	1 38
24	1 0 47493 1 2 1040	58   0.49604   2.01596 00   0.49640   2.01449	1 0.51/98   1.9305/	0.54032   1.85075	0.56309   1.77592	1 37
25	1 0.47519 1 2.1044	12   0.49677   2.01302	1 0.31833   1.72720	1 0.540/0 1 1.84946	1 0.3634/   1.//4/1	1 36
26	1 0.47555 1 2.1026	34   0.49713   2.01155	1 0.310/2   1.72/02	1 0 54 145 1 1 84488	1 0.36363   1.77331	33
27	1 0.47590 1 2.1012	26   0.49749   2.0100B	I 0.51946 I 1.92508	1 0.54183   1.84541	1 0 54442   1 77110	1 37
28	1 0.47626 1 2.0996	9   0.49786   2.00862	I 0.51983   1.92371	1 0.54220 1 1.84433	1 0.56501 I 1.76990	1 32
29	1 0.47662   2.098	11   0.49822   2.00715	0.52020   1.92235	1 0.54258   1.84305	1 0.56539 1 1.76869	1 31
130	1 0.47698   2.096	54   0.49858   2.00569	1 0.52057   1.92098	1 0.54296 I 1.84177	1 0.54577 1 1.74749	ו סדי
[31	1 0.47733   2.0949	PB   0.49894   2.00423	1 0.52094 1 1.91962	1 0.54333   1.84049	1 0.56616 J 1.76629	1 29
32	1 0.47769 1 2.0934	1   0.49931   2.00277	1 0.52131 1 1.91826	0.54371   1.83922	0.56654   1.76510	1 28
22	0.47805   2.0918	34   0.49967   2.00131	1 0.52168 1 1.91690	1 0.54409   1.83794	1 0.56693 1 1.76390	1 27
34	0.47840   2.0902	28   0.50004   1.99986	1 0.52205   1.91554	1 0.54446   1.83667	1 0.56731   1.76271	1 26
33	0.47876   2.0887	72   0.50040   1.99841	1 0.52242   1.91418	1 0.54484   1.83540	0.56769   1.76151	1 25
36	1 0.47912 1 2.087	16   0.50076   1.99695	1 0.52279   1.91282	1 0.54522   1.83413	1 0.56808   1.76032	1 24
3/	1 0 47994 1 2 004	50   0.50113   1.99550	0.52316   1.91147	1 0.54560   1.83286	0.56846   1.75913	1 23
30	1 0 48019 1 2 083	05   0.50149   1.99406 50   0.50185   1.99261	0.52353   1.91012	0.54597   1.83159	0.56885   1.75794	1 22
40	1 0.48055 1 2 0805	74   0.50222   1.99116	1 0.52390   1.908/6	0.54635   1.83033	0.56923   1.75675	1 21
41	1 0.48091 1 2.079	39   0.50258   1.98972	1 0.52427   1.70741	0.546/3   1.82906	0.56962   1.75556	1 20
42	1 0.48127 1 2.0778	5   0.50295   1.98828	1 0.52501 1 1.90472	1 0.54711   1.82760	1 0.57000   1.75437	1 19
143	1 0.48163 1 2.076	30   0.50331   1.98684	1 0.52538   1.90337	I 0.54786 I 1 82528	1 0 57078 1 1 75200	1 17
177	1 0.48198 1 2.074	76   0.50368   1.98540	1 0.52575 1 1.90203	1 0.54824 1 1.82402	1 0.57116 1 1 75082	1 14
143	1 0.48234 1 2.073	21   0.50404   1.98396	I 0.52613 I 1.90069	1 0.54842 1 1 82274	1 0 57155 1 1 74044	1 15
140	1 0.48270 1 2.071	57   0.50441   1.9B253	1 0.52650 I 1.89935	1 0.54900 1 1 82150	1 0 5710% 1 1 7404A	1 14
147	1 0.48306 1 2.070	14   0.50477   1.98110	1 0.52687   1.89801	1 0.54938 1 1.82025	1 0 57732 1 1 74720	1 17
140	1 0.48342   2.068	50   0.50514   1.97966	.   0.52724   1.89667	1 0.54975   1.81899	1 0.57271 1 1 74410	1 12
147	1 0.48378 1 2.0670	06   0.50550   1.97823	1 0.52761 1 1.89533	I 0.55013 I 1.81774	1 0.57309 I 1.74492	1 11
30	1 0 48450 1 2 044	53   0.50587   1.97681	1 0.52798   1.89400	1 0.55051   1.81649	1 0.57348   1.74375	1 10
52	1 0.48486 1 2 042	00   0.50623   1.97538 47   0.50660   1.97395	1 0.32836   1.89266	0.55089   1.81524	1 0.57386   1.74257	1 9
53	1 0.48521 1 2.040	94   0.50696   1.97395	1 0.528/3   1.89133	1 0.33127   1.81399	1 0.57425   1.74140	! 8
54	1 0.48557 1 2.059	42   0.50733   1.97111	1 0.34710   1.87000	1 0.33163   1.81274	1 0.3/464   1.74022	1 7
55	1 0.48593 1 2.057	90   0.50769   1.96969	1 0.52985 1 1 99734	1 0.33203   1.81130	1 0.3/303   1./3903	1 6
36	1 0.48629 1 2.056	37   0.50806   1.96827	1 0.53022   1.88602	1 0.55279 1 1.80901	1 0.57580 I 1.73A71	1 4
12/	1 0.48663   2.054	85   0.50843   1.96685	1 0.53059 1 1.88469	1 0.55317 1 1.80777	1 0 57419 1 1 77555	
128	1 0.48701 1 2.053	33   0.50879   1.96544	1 0.53096 1 1.88337	1 0.55355 L 1.80A53	1 0.57657 1 1.73439	1 2
137	1 0.48/3/ 1 2.051	82   0.50916   1.96402	0.53134   1.88205	1 0.55393 1 1.80529	1 0.57494 1 1 73391	1 1
60	0.48//3 1 2.050	30   0.50953   1.96261	1 0.53171 1 1.88073	0.55431   1.80405	I 0.57735 I 1.73205	ıō
1						
		N COT TAN		_ — — — — — — —	COT TAN	
	64*	63°	62.	<b>61°</b>	60*	7
1						
L						

Table AII-2.—Natural Tangents and Cotangents—Continued

Γ											
	30		31	<u></u>	32		 33	<del></del>	34	<del></del>	
I											- 1
2	TAN	COT	TAN	COT	TAN	_co.r	TAN	COT	TAN	COT	
0	0.57735	1.73205	0.60086	1.66428	0.62487	1.60033	1 0.64941 1	1.53986	1 0.67451 1	1.48256	1 60
							1 0.64982 !				
							0.65024 1				
							0.65065 1				
							1 0.65106 I				
							0.65148     0.65189				
							0.65231				
							0.65272 1				
							i 0.65314 I				
							1 0.65355 1				
							1 0.65397 1				1 49
							1 0.65438 1				
							0.65480				
							0.65521     0.65563				
							1 0.65604 1				
							1 0.65646 1				
							1 0.65688 1				
							1 0.65729 1				
							1 0.65771 1				
							0.65813				1 39
							1 0.65854 1				
							1 0.65938 1				
							1 0.65980 1				
							1 0.66021				
27	1 0.58787 1	1.70106	0.61160	1.63505	1 0.63584 1	1.57271	1 0.66063 1	1.51370	0.68600	1.45773	1 32
							1 0.66105 1				
							1 0.66147 1				
							0.66189				
ı							1 0.66230				
							1 0.66314				
							1 0.66356				
							1 0.66398				
							1 0.66440				
							1 0.66482				
							1 0.66524				
							1 0.66566				
							1 0.6660B				
							1 0.66650				
							1 0.66734				
							1 0.66776				
45	1 0.59494	1.68085	0.61882	1.61598	1 0.64322	1.55467	0.66818	1.49661	1 0.69372	1.44149	1 15
							0.66860				
							1 0.66902				
							0.66944				
							1 0.67028				
51	0.59730	1.67419	1 0.62124	1.60970	1 0.64569	1.54873	1 0.67071	1.49097	1 0.69631	1.43614	1 9
52	1 0.59770	1.67309	0.62164	1.60865	1 0.64610	1.54774	1 0.67113	1 1.49003	1 0.69675	1 1.43525	1 8
53	0.59809	1 1.67198	0.62204	1.60761	0.64652	1.54675	0.67155	1.48909	1 0.69718	1 1.43436	1 7
54	0.59849	1.67088	0.62245	1 1.60657	1 0.64693	1 1.54576	1 0.67197	1 1.48816	0.69761	1 1.43347	1 6
							1 0.67239				
							1 0.67282				
							1 0.67366				
59	1 0.60046	1 1.66538	1 0.62446	1 1.60137	1 0.64899	1 1.54085	1 0.67409	1 1.48349	1 0.69977	1 1.42903	1 1
60	1 0.60086	1.66428	1 0.62487	1.60033	1 0.64941	1.53986	1 0.67451	1 1.48256	1 0.70021	1.42815	1 ō
		TAN					COT				- I
	59	<b>&gt; -</b>	56	3 *	57	-	54	<b>-</b>	55	5 ~	7

Table AII-2.—Natural Tangents and Cotangents—Continued

<u></u>	35	-	36	•	37	-	38	•	39	•	
N I	TAN	COT	TAN	COT	TAN	COT	TAN	COT	TAN	COT	1
0 1	0.70021 1	1.42815	0.72654 1	1.37638 (	0.75355 1	1.32704 1	0.78129	1.27994	0.80978 1	1.23490	60
			0.72699 1								59
2 1	0.70107 l	1.42638	0.72743	1.37470	0.75447 1	1.32544	0.78222 1	1.27841	0.81075 I	1.23343 1	58
			0.72788								
4 1	0.70194	1.42462	0.72832	1.37302	0.75538	1.32384	0.78316	1.27688	0.81171	1.23196	
			0.72877								55
			0.72921   0.72966								
			0.73010								
			0.73055								
			0.73100								
			0.73144								
			0.73189								
			0.73234								
			0.73278								
			0.73323								
			0.73368 1								
			0.73413								
			0.73457								
			1 0.73502 1								
			0.73547								
			1 0.73592 1								1 39
			1 0.73637 1								1 28
			1 0.736B1 1								
			1 0.73726 1								
			1 0.73771 1								
			I 0.73816 J								
27	0.71198	1.40454	1 0.73861 1	1.35389	1 0.76594	1.30558	0.79401	1.25943	1 0.82287 1	1.21526	1 22
28	0.71242	1.40367	1 0.73906 1	1.35307	1 0.76640	1.30480	1 0.79449	1.25867	1 0.82336 1		1 32
			1 0.73951 1							1.21382	
			1 0.73996 1								
31	0.71373	1.40109	1 0.74041 1	1.35060	1 0.76779	1.30244	1 0.79591	1.25642	1.0.82483	1.21238	1 29
32	1 0.71417	1.40022	1 0.74086	1.34978	1 0.76825	1.30166	1 0.79639	1.25567	0.82531	1.21166	1 58
33	0.71461	1.39936	1 0.74131	1.34896	0.76871	1.30087	0.79686	1.25492	0.82580	1.21094	1 27
34	1 0.71505	1 1.39850	1 0.74176	1.34814	1 0.76918	1 1.30009	1 0.79734	1.25417	1 0.82629	1.21023	1 26
35	0.71549	1.39764	1 0.74221	1.34732	1 0.76964	1.29931	0.79781	1.25343	0.82678	1.20951	1 23
36	0.71593	1.39679	1 0.74267	1.34650	1 0.77010	1.29853	0.79829	1.25268	0.82727	1.208/9	1 24
			0.74312								
			1 0.74357								
			1 0.74442								
			1 0.74492								1 19
			1 0.74538								
43			1 0.74583								
			1 0.74628								
45			1 0.74674								
			1 0.74719								
			1 0.74764								
			0.74810								
			0.74855								
			1 0.74900								
			1 0.74946								
			0.74991								
			1 0.75037								
			1 0.75082								
55	1 0.72432	1 1.38060	1 0.75128	1 1.33107	1 0.77895	1 1.28379	1 0.80738	1 1.23858	1 0.83662	1 1.19528	1 5
56	1 0.72477	1 1.37976	1 0.75173	1 1.33026	1 0.77941	1 1.28302	1 0.80786	1 1.23784	1 0.83712	1 1.19457	1 4
57	1 0.72521	1 1.37891	1 0.75219	1 1.32946	1 0.77988	1 1.28225	1 0.80834	1 1.23710	I 0.83761	1 1.19387	1 3
58	1 0.72565	1 1.37807	1 0.75264	1 1.32865	1 0.78035	1 1.28148	1 0.80882	1.23637	0.83811	1 1.19316	1 2
59	1 0.72610	1.37722	1 0.75310	1 1.32785	1 0.78082	1 1.28071	1 0.80930	1.23563	0.83860	1 1.19246	1 1
60			0.75355								
	COT	TAN	COT	TAN	COT		COT	TAN	COT	TAN	۳ ت
1	25.	4-	5	<b>5</b> *	5		5	1 *	50	> <del>-</del>	
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1											

Table AII-2.—Natural Tangents and Cotangents—Continued

	40*	41*	42*	43*	44-	
I	TAN COT	TAN COT	TAN COT	TAN COT	TAN COT	.
z						
0 i	0.83910   1.19175	0.86929   1.15037	0.90040   1.11061	0.93252   1.07237	1 0.96569   1.03553	1 60
1 1	0.83760   1.17105	0.86980   1.14969	0.90093   1.10998	0.93306   1.07174	0.76623   1.03473	
2 1	0.84009   1.17035	0.87082   1.14834	0.90199   1.10967	0.93415   1.07049	0.96738   1.03372	57
4	0.84108   1.18894	0.87133   1.14767	0.90251   1.10802	0.93469   1.06987	1 0.96794   1.03312	
5 1	0.84158   1.18824	0.87184   1.14699	0.90304   1.10737	0.93524   1.06925	0.96850   1.03252	1 55
۱ ۸ ۱	0.84208   1.18754	0.87236   1.14632	0.90357   1.10672	0.93578   1.06862	1 0.96907 1 1.03192	1 54
7 1	0.84258   1.18684	0.87287   1.14565	0.90410   1.10607	0.93633   1.06800	0.96963   1.03132	53
8	0.84307   1.18614	0.87338   1.14498	0.90463   1.10543	0.93688   1.06/38	! 0.97020   1.03072   0.97076   1.03012	1 32
10	0.8433/	0.87384   1.14430	0.90549   1.104/4	0.93797   1.06613	1 0.97133   1.02952	50
1 10	0.84457   1.18404	0.87492   1.14296	0.90621   1.10349	0.93852   1.04551	1 0.97189   1.02892	1 49
12 1	1 0.84507   1.18334	! 0.87543   1.14229	0.90674   1.10285	0.93906   1.06489	1 0.97246   1.02832	1 48
13	0.84556   1.18264	0.87 <b>595</b>   1.14162	0.90727   1.10220	0.93961   1.06427	1 0.97302   1.02772	1 47
14 1	1 0.84606 1 1.18194	1 0.87646   1.14095	0.90781   1.10154	0.94016   1.06365	1 0.97359   1.02713	1 46
15	0.84656   1.18125	0.87698   1.14028	0.90834   1.10091	0.94071   1.06303	1 0.97416   1.02653	1 45
16	1 0.84706   1.18055	1 0.87/49   1.13961	0.90940   1.10027	0.74123   1.06241   0.94180   1.04179	0.97472   1.02593   0.97529   1.02533	1 47
16	1 0.84806 1 1 17914	1 0.87852 1 1.13879	0.90993   1.07899	0.94235   1.06117	1 0.97586   1.02474	1 42
					I 0.97643 I 1.02414	
20	I 0.84906   1.17777	1 0.87955 1 1.13694	0.91099   1.09770	1 0.94345   1.05994	0.97700   1.02355	1 40
21	1 0.84956   1.17708	1 0.88007 1 1.13627	0.91153   1.09706	0.94400   1.05932	1 0.97756   1.02295	1 39
22	0.85006   1.17638	0.88059   1.13561	0.91206   1.09642	0.94455   1.05870	0.97813   1.02236   0.97870   1.02176	1 38
23	1 0.8505/   1.1/569	0.88110   1.13474   0.88162   1.13428	0.91313   1.09514	1 0.94565   1.05747	1 0.97927   1.02117	1 36
25	1 0.85157   1.17430	0.88214   1.13361	0.91366   1.09450	1 0.94620 1 1.05685	1 0.97984 1 1.02057	1 35
		1 0.88265   1.13295				1 34
27	I 0.85257 I 1.17292	0.88317   1.13228	0.91473   1.09322	1 0.94731 ! 1.05562	1 0.98098   1.01939	
28	1 0.85308 1 1.17223	0.88369   1.13162	0.91526   1.09258	1 0.94786   1.05501	1 0.98155 1 1.01879	1 32
29	0.85358   1.17154	0.88421   1.13096	0.91580   1.09195	1 0.94841   1.05439	1 0.98213   1.01820	1 31
30	1 0.85408   1.17085	0.884/3   1.13029	1 0.91633 1 1.09131	1 0.74876 1 1.05378	0.98270   1.01761   0.98327   1.01702	1 29
					1 0.98384   1.01642	
					1 0.98441   1.01583	
34	1 0.85609   1.16809	1 0.88680   1.12765	1 0.91847   1.08876	1 0.95118   1.05133	1 0.98499 1 1.01524	1 26
					1 0.98556   1.01465	
					1 0.98613   1.01406	
					i 0.98671   1.01347   0.98729   1.01298	
10	0.83811   1.16333	1 0.88940   1.12301	1 0.92116 1 1.08559	1 0.75370   1.04827	1 0.98786   1.01229	1 21
					1 0.98843   1.01170	
41	1 0.85963   1.16329	I 0.89045 I 1.12303	1 0.92224 1 1.08432	I 0.95506   1.04705	0.98901   1.01112	1 19
					1 0.98958 ! 1.01053	
					1 0.99016   1.00994	
					1 0.99073 1 1.00935	
					1 0.99189   1.00818	
					1 0.99247 1 1.00759	
48	1 0.86318   1.15851	1 0.89410 1 1.11844	1 0.92601   1.07990	1 0.95897   1.04279	1 0.99304   1.00701	1 12
					1 0.99362   1.00642	
					1 0.99420 1 1.00583	
					1 0.99536 1 1.00467	
		1 0.89672   1.11517				i 7
54	1 0.86623 1 1.15443	1 0.89725 1 1.11452	1 0.92926 1 1.07613	1 0.96232   1.03915	1 0.99652 1 1.00350	
55	1 0.86674   1.15375	1 0.89777   1.11387	1 0.92980   1.07550	1 0.96288   1.03855	1 0.99710   1.00291	1 5
					1 0.99768   1.00233	
					1 0.99884   1.00175	
					1 0.99942   1.00058	
					1 1.00000 1 1.00000	
			COT TAN		COT TAN	- M
1	49*	48*	47°	46*	45°	7 7
1						

**Table AII-3.—Stadia Reduction** 

	0	•	1'	•	2	•	3	
Minutes	Hor.	Diff.	Hor.	Diff. elev.	Hor. dist.	Diff. elev.	Hor.	Diff.
	dist.	elev.	dist.	elev.	Gist.	——————————————————————————————————————		
0	100.00	0.00	99.97	1.74	99.88	3.49	99.73	5.23
2	100.00	0.06	99.97	1.80	99.87	3.55	99.72	5.28
4	100.00	0.12	99.97	1.86	99.87	3.60	99.71	5.34
6	100.00	0.17	99.96	1.92	99.87	3.66	99.71	5.40
8	100.00	0.23	99.96	1.98	99.86	3.72	99.70	5.46
10	100.00	0.29	99.96	2.04	99.86	3.78	99.69	5.52
12	100.00	0.35	99.96	2.09	99.85	3.84	99.69	5.57
14	100.00	0.41	99.95	2.15	99.85	3.90	99.68	5.63
16	100.00	0.47	99.95	2.21	99.84	.3.95	99.68	5.69
18	100.00	0.52	99.95	2.27	99.84	4.01	99:67	5.78
20	100:00	0.58	99.95	2.33	99.83	4.07	99.66	5.80
22	100.00	0.64	99.94	2.38	99.83	4.13	99.66	5.80
24	100.00	0.70	99.94	2.44	99.82	4.18	99.65	5.9
26	99.99	0.76	99.94	2.50	99.82	4.24	99.64	5.9
28	99.99	0.81	99.93	2.56	99.81	4.30	99.63	6.0
30	99.99	0.87	99.93,	2.62	99.81	4.36	99.63	6.0
32	99.99	0.93	99.93	2.67	99.80	4.42	99.62	6.1
34	99.99	0.99	99.93	2.73	99.80	4.48	99.62	6.2
36	99.99	1.05	99.92	2.79	99.79	4.53	99.61	6.2
38	99.99	1.11	99.92	2.85	99.79	4.59	99.60	6.3
40	99.99	1.16	99.92	2.91	99.78	4.65	99.59	6.3
42	99.99	1.22	99.91	2.97	99.78	4.71	99.59	6.4
44	99.98	1.28	99.91	3.02	99.77	4.76	99.58	6.5
46	99.98	1.34	99.90	3.08	99.77	4.82	99.57	6.5
48	99.98	1.40	99.90	3.14	99.76	4.88	99.56	6.6
50	99.98	1.45	99.90	3.20	99.76	4.94	99.56	6.6
52	99.98	1.51	99.89	3.26	99.75	4.99	99.55	6.7
54	99.98	1.57	99.89	3.31	99.74	5.05	99.54	6.7
56	99.97	1.63	99.89	3.37	99.74	5.11	99.53	6.8
58	99.97	1.69	99.88	3.43	99.73	5.17	99.52	6.9
60	99.97	1.74	99.88	3.49	99.73	5.23	99.51	6.9
C=0.75	0.75	0.01	0.75	0.02	0.75	0.03	0.75	0.0
C=1.00	1.00	0.01	1.00	0.03	1.00	0.04	1.00	0.0
C=1.25	1.25	0.02	1.25	0.03	1.25	0.05	1.25	0.0

Table AII-3.—Stadia Reduction—Continued

	4	•	5	•	6	•	7	•
Minutes	Hor. dist.	Diff. elev.	Hor. dist.	Diff. elev.	Hor. dist.	Diff. elev.	Hor. dist.	Diff. elev.
0	99.51	6.96	99.24	8.68	98.91	10.40	98.51	12.10
2	99.51	7.02	99.23	8.74	98.90	10.45	98.50	12.15
4	99.50	7.07	99.22	8.80	98.88	10.51	98.48	12.21
6	99.49	7.13	99.21	8.85	98.87	10.57	98.47	12.26
8	99.48	7.19	99.20	8.91	98.86	10.62	98.46	12.32
10	99.47	7.25	99.19	8.97	98.85	10.68	98.44	12.38
2	99.46	7.30	99.18	9.03	98.83	10.74	98.43	12.43
14	99.46	7.36	99.17	9.08	98.82	10.79	98.41	12.49
6	99.45	7.42	99.16	9.14	98.81	10.85	98.40	12.55
8	99.44	7.48	99.15	9.20	98.80	10.91	98.39	12.60
20	99.43	7.53	99.14	9.25	98.78	10.96	98.37	12.66
22	99.42	7.59	99.13	9.31	98.77	11.02	98.36	12.72
4	99.41	7.65	99.11	9.37	98.76	11.08	98.34	12.77
8	99.40	7.71	99.10	9.43	98.74	11.13	98.33	12.83
8	99.39	7.76	99.09	9.48	98.73	11.19	98.31	12.88
0	99.38	7.82	99.08	9.54	98.72	11.25	98.29	12.94
2	99.38	7.88	99.07	9.60	98.71	11.30	98.28	13.00
4	99.37	7.94	99.06	9.65	98.69	11.36	98.27	13.05
8	99.36	7.99	99.05	9.71	98.68	11.42	98.25	13.11
8	99.35	8.05	99.04	9.77	98.67	11.47	98.24	13.17
0	99.34	8.11	99.03	9.83	98.65	11.53	98.22	13. <b>22</b>
2	99.33	8.17	99.01	9.88	98.64	11.59	98.20	13. <b>2</b> 8
4	99.32	8.22	99.00	9.94	98.63	11.64	98.19	13.33
6	99.31	8.28	98.99	10.00	98.61	11.70	98.17	13.39
8	99.30 99.29	8.34 8.40	98.98 98.97	10.05 10.11	98.60 98.58	11.76 11.81	98.16 98.14	13.45 13.50
2						l		
4	99.28 99.27	8.45 8.51	98.96 98.94	10.17 10.22	98.57	11.87	98.13	13.56
6	99.26	8.57	98.94 98.93	10.22	98.56 98.54	11.93 11.98	98.11 98.10	13.61 13.67
8	99.25	8.63	98.92	10.28	98.53	12.04	98.08	13.73
00	99.24	8.68	98.91	10.40	98.51	12.10	98.06	13.78
C=0.75	0.75	0.06	0.75	0.07	0.75	0.08	0.74	0.10
C=1.00	1.00	0.08	0.99	0.09	0.99	0.11	0.99	0.13
C = 1.25	1.25	0.10	1.24	0.11	1.24	0.14	1.24	0.16

Table AII-3.—Stadia Reduction—Continued

	8	•	9'	•	10	•	11	•
Minutes	Hor. dist.	Diff. elev.	Hor. dist.	Diff. elev.	Hor. dist.	Diff. elev.	Hor. dist.	Diff.
0	98.06	13.78	97.55	15.45	96.98	17.10	96.36	18.73
2	98.05	13.84	97.53	15.51	96.96	17.16	96.34	18.78
4	98.03	13.89	97.52	15.56	96.94	17.21	96.32	18.84
6	98.01	13.95	97.50	15.62	96.92	17.26	96.29	18.89
8	98.00	14.01	97.48	15.67	96.90	17.32	96.27	18.98
0	97.98	14.06	97.46	15.73	96.88	17.37	96.25	19.00
2	97.97	14.12	97.44	15.78	96.86	17.43	96.23	19.0
4	97.95	14.17	97.43	15.84	96.84	17.48	96.21	19.1
6	97.93	14.23	97.41	15.89	96.82	17.54	96.18	19.10
8	97.92	14.28	97.39	15.95	96.80	17.59	96.16	19.21
0	97.90	14.34	97.37	16.00	96.78	17.65	96.14	19.27
22	97.88	14.40	97.35	16.06	96.76	17.70	96.12	19.32
4	97.87	14.45	97.33	16.11	96.74	17.76	96.09	19.3
6	97.85	14.51	97.31	16.17	96.72	17.81	96.07	19.4
8	97.83	14.56	97.29	16.22	96.70	17.86	96.05	19.4
0	97.82	14.62	97.28	16. <b>28</b>	96.68	17.92	96.03	19.54
2	97.80	14.67	97. <b>2</b> 6	16.33	96.66	17.97	96.00	19.5
4	97.78	14.73	97.24	16.39	96.64	18.03	95:98	19.6
6	97.76	14.79	97.22	16.44	96.62	18.08	95.96	19.7
8	97.75	14.84	97.20	16.50	96.60	18.14	95.93	19.7
.0	97.73	14.90	97.18	16.55	96.57	18.19	95.91	19.8
2	97.71	14.95	97.16	16.61	96.55	18.24	95.89	19.8
4	97.69	15.01	97.14	16.66	96.53	18.30	95.86	19.9
6	97.68	15.06	97.12	16.72	96.51	18.35	95.84	19.9
18	97.66	15.12	97.10	16.77	96.49	18.41	95.82	20.0
50	97.64	15.17	97.08	16.83	96.47	18.46	95.79	20.0
2	97.62	15.23	97.06	16.88	96.45	18.51	95.77	20.1
4	97.61	15.28	97.04	16.94	96.42	18.57	95.75	20.1
6	97.59	15.34	97.02	16.99	96.40	18.62	95.72	20.2
8	97.57	15.40	97.00	17.05	96.38	18.68	95.70	20.2
	97.55	15.45	96.98	17.10	96.36	18.73	95.68	20.3
C=0.75	0.74	0.11	0.74	0.12	0.74	0.14	0.73	0.1
C = 1.00	0.99	0.15	0.99	0.16	0.98	0.18	0.98	0.2
C=1.25	1.23	0.18	1.23	0.21	1.23	0.23	1.22	0.2

Table AII-3.—Stadia reduction—Continued

	12	3°	13	3°	14	•	15	•
Minutes	Hor. dist.	Diff. elev.	Hor. dist.	Diff. elev.	Hor. dist.	Diff. elev.	Hor. dist.	Diff. elev.
0	95.68	20.34	94.94	21.92	94.15	23.47	93.30	25.00
2	95.65	20.39	94.91	21.97	94.12	23.52	93.27	25.05
4	95.63	20.44	94.89	22.02	94.09	23.58	93.24	25.10
8	95.61	20.50	94.86	22.08	94.07	23.63	93.21	25.15
8	95.58	20.55	94.84	22.13	94.04	23.68	93.18	25.20
0	95.56	20.60	94.81	22.18	94.01	23.73	93.16	25.25
2	95.53	20.66	94.79	22.23	93.98	23.78	93.13	25.30
<b>4</b>	95.51	20.71	94.76	22.28	93.95	23.83	93.10	25.35
3	95.49	<b>2</b> 0.76	94.73	22.34	93.93	23.88	93.07	25.40
3	95.46	20.81	94.71	22.39	93.90	<b>23</b> .93	93.04	25.48
0	95.44	20.87	94.68	22.44	93.87	23.99	93.01	25.50
2	95.41	20.92	94.66	22.49	93.84	24.04	92.98	25.5
<b>4</b> [	95.39	20.97	94.63	22.54	93.81	24.09	92.95	<b>25</b> . <b>6</b> 0
8	95.36	21.03	94.60	22.60	93.79	24.14	92.92	25.65
3	95.34	21.08	94.58	22.65	93.76	24.19	92.89	<b>25</b> .70
0	95.32	21.13	94.55	22.70	93.73	24.24	92.86	25.75
2	95.29	21.18	94.52	22.75	93.70	24.29	92.83	25.80
4	95.27	21.24	94.50	22.80	93.67	24.34	92.80	25.85
§	95.24	21.29	94.47	22.85	93.65	24.39	92.77	25.90
8	95.22	21.34	94.44	<b>22</b> .91	93.62	24.44	92.74	25.95
0	95.19	21.39	94.42	22.96	93.59	24.49	92.71	26.00
2	95.17	21.45	94.39	<b>2</b> 3.01	93.56	24.55	92.68	26.05
<b>5</b>	95.14	21.50	94.36	23.06	93.53	24.60	92.65	26.10
6	95.12	21.55	94.34	23.11	93.50	24.65	92.62	26.15
8	95.09	21.60	94.31	23.16	93.47	24.70	92.59	<b>2</b> 6. <b>2</b> 0
0	95.07	21.66	94.28	23.22	93.45	24.75	92.56	26.25
2	95.04	21.71	94.26	23.27	93.42	24.80	92.53	26.30
4	95.02	21.76	94.23	23.32	93.39	24.85	92.49	26.35
6	94.99	21.81	94.20	23.37	93.36	24.90	92.46	26.40
8	94.97	21.87	94.17	23.42	93.33	24.95	92.43	26.45
0	94.94	21.92	94.15	23.47	93.90	25.00	92.40	26.50
=0.75	0.73	0.16	0.73	0.17	0.73	0.19	0.72	0.20
=1.00	0.98	0.22	0.97	0.23	0.97	0.25	0.96	0.27
=1.25	1.22	0.27	1.21	0.29	1.21	0.31	1.20	0.34

Table AII-3.—Stadia Reduction—Continued

_	16	•	17	•	18°		19	) <b>•</b>
Minutes	Ног.	Diff.	Hor.	Diff.	Hor.	Diff.	Hor.	Diff.
	dist.	elev.	dist.	elev.	dist.	elev.	dist.	elev.
D	92.40	26.50	91.45	27.96	90.45	29.39	89.40	30.78
2	92.37	26.55	91.42	28.01	90.42	29.44	89.36	30.83
6	92.34	<b>2</b> 6. <b>5</b> 9	91.39	28.06	90.38	29.48	89.33	30.87
В	92.31	26.64	91.35	28.10	90.35	29.53	89.29	30.92
B	92.28	26.69	91.32	28.15	90.31	29.58	89.26	30.97
)	92.25	26.74	91. <b>2</b> 9	28.20	90.28	29.62	89.22	31.01
	92.22	26.79	91.26	28.25	90.24	29.67	89.18	31.06
	92.19	26.84	91.22	28.30	90.21	29.72	89.15	31.10
	92.15	<b>26.8</b> 9	91.19	28.34	90.18	29.76	89.11	31.15
3	92.12	26.94	91.16	28.39	90.14	29.81	89.08	31.19
):	92.09	26.99	91.12	28.44	90.11	29.86	89.04	31.24
	92.06	27.04	91.09	28.49	90.07	29.90	89.00	31.28
	92.03	27.09	91.06	28.54	90.04	29.95	88.96	31.33
	92.00	27.13	91.02	28.58	90.00	30.00	88.93	31.38
	91.97	27.18	90.99	28.63	89.97	30.04	88.89	31.42
	91.93	27.23	90.96	28.68	89.93	30.09	88.86	31.47
	91.90	27.28	90.92	28.73	89.90	30.14	88.82	31.51
	91.87	27.33	90.89	28.77	89.86	30.19	88.78	31.50
	91.84	27.38	90.86	28.82	89.83	30.23	88.75	31.60
	91.81	27.43	90.82	28.87	89.79	30.28	88.71	31.6
)	91.77	27 . 48	90.79	28.92	89.76	30.32	88.67	31.69
	91.74	27.52	90.76	28.96	89.72	30.37	88.64	31.74
••••	91.71	27.57	90.72	29.01	89.69	30.41	88.60	31.78
	91.68	27.62	90.69	29.06	89.65	30.46	88.56	31.83
	91.65	27.67	90.66	29.11	89.61	30.51	88.53	31.87
)	91.61	27.72	90.62	29.15	89.58	30.55	88.49	31.92
	91.58	27.77	90.59	29.20	89.54	30.60	88.45	31.96
	91.55	27.81	90.55	29.25	89.51	30.65	88.41	32.01
	91.52	27.86	90.52	29.30	89.47	30.69	88.38	32.05
	91.48	27.91	90.48	29.34	89.44	30.74	88.34	32.09
	91.45	27.96	90.45	29.39	89.40	30.78	88.30	32.14
-0.75	0.72	0.21	0.72	0.23	0.71	0.24	0.71	0.25
-1.00	0.96	0.28	0.95	0.30	0.95	0.32	0.94	0.33
<b>-</b> 1.25	1.20	0.35	1.19	0.38	1.19	0.40	1.18	0.42

Table AII-3.—Stadia Reduction—Continued

	20	)•	21	•	22	<b>!•</b>	23	•
Minutes	Hor. dist.	Diff. elev.	Hor. dist.	Diff. elev.	Hor. dist.	Diff. elev.	Hor. dist.	Diff.
0	88.30	32.14	87.16	33.46	85.97	34.73	84.73	35.97
2	88.26	32.18	87.12	33.50	85.93	34.77	84.69	36.01
4	88.23	32.23	87.08	33.54	85.89	34.82	84.65	36.05
6	88.19	32.27	87.04	33.59	85.85	34.86	84.61	36.09
B	88.15	32.32	87.00	33.63	85.80	34.90	84.57	36.13
0	88.11	32.36	86.96	33.67	85.76	34.94	84.52	36.17
3	88.08	32.41	86.92	33.72	85.72	34.98	84.48	36.2
4	88.04	32.45	86.88	33.76	85.68	35,02	84.44	36.2
3	88.00	32.49	86.84	33.80	85.64	35.07	84.40	36.29
B	87.96	32.54	86.80	33.84	85.60	35.11	84.35	36.3
D	87.93	32.58	86.77	33.89	85.56	35.15	84.31	36.3
3	87.89	32.63	86.73	33.93	85.52	35.19	84.27	36.4
	87.85	32.67	86.69	33.97	85.48	<b>35.23</b>	84.23	36.4
	87.81	32.72	86.65	34.01	85.44	35.27	84.18	36.4
	87.77	32.76	86.61	34.06	85.40	35.31	84.14	36.5
	87.74	32.80	86.57	34.10	85.36	35.36	84.10	36.5
	87.70	32.85	86.53	34.14	85.31	35.40	84.06	36.6
	87.66	32.89	86.49	34.18	85.27	35.44	84.01	36.6
	87.62	32.93	86.45	34.23	85.23	35.48	83.97	36.6
	87.58	32.98	86.41	34.27	85.19	35.52	83.93	36.7
·	87.54	33.02	86.37	34.31	85.15	35.56	83.89	36.7
	87.51	33.07	86.33	34.35	85.11	35.60	83.84	36.8
	87 . 47	33.11	86.29	34.40	85.07	35.64	83.80	36.8
	87.43	33.15	86.25	34.44	85.02	35.68	83.76	36.8
3	87.39	33.20	86.21	34.48	84.98	35.72	83.72	36.9
)	87.35	33.24	86.17	34.52	84.94	35.76	83.67	36.90
	87.31	33.28	86.13	34.57	84.90	35.80	83.63	37.0
	87.27	33.33	86.09	34.61	84.86	35.85	83.59	37.0
3	87.24	33.37	86.05	34.65	84.82	35.89	83.54	37.0
3	87.20	33.41	86.01	34.69	84.77	35.93	83.50	37.12
),  	87.16	33.46	85.97	34.73	84.73	35.97 	83.46	37.10
=0.75	0.70	0.26	0.70	0.27	0.69	0.29	0.69	0.30
-1.00	0.94	0.35	0.93	0.37	0.92	0.38	0.92	0.40
<b>-</b> 1.25	1.17	0.44	1.16	0.46	1.15	0.48	1.15	0.5

Table AII-3.—Stadia Reduction—Continued

	2-		2.	5°	26°		27	•
Minuter	Hor.	Diff.	Hor.	Diff.	Hor.	Diff.	Hor.	Diff.
	dist.	elev.	dist.	elev.	dist.	elev.	dist.	elcv.
0	83.46	37.16	82.14	38.30	80.78	39.40	79.39	40.45
2	83.41	37.20	82.09	38.34	80.74	39.44	79.34	40.49
4	83.37	37.23	82.05	38.38	80.69	39.47	79.30	40.52
6	83.33	37.27	82.01	38.41	80.65	39.51	79.25	40.55
8	83.28	37.31	81.96	38.45	80.60	39.54	79.20	40.59
0	83. <b>24</b>	37.35	81.92	38.49	80.55	39.58	79.15	40.62
2	83. <b>2</b> 0	37.39	81.87	38.53	80.51	39.61	79.11	40.66
·	83.15	37.43	81.83	38.56	80.46	39.65	79.06	40.69
B	83.11	37.47	81.78	38.60	80.41	39.69	79.01	40.72
8	83.07	37.51	81.74	38.64	80.37	39.72	78.96	40.76
0	83.02	37.54	81.69	38.67	80.32	39.76	78.92	40.79
2	82.98	37.58	81.65	38.71	<b>8</b> 0. <b>2</b> 8	39.79	78.87	40.82
4	82.93	37.62	81.60	38.75	80.23	39.83	78.82	40.86
6	82.89	37.66	81.56	38.78	80.18	39.86	78.77	40.89
3	82.85	37.70	81.51	38.82	80.14	39. <b>90</b> .	78.73	40.92
0	82.80	37.74	81.47	38.86	80.09	39.93	78.68	40.96
2	82.76	37.77	81.42	38.89	80.04	39.97	78.63	40.99
4	82.72	37.81	81.38	38.93	80.00	40.00	78:58	41.0
6	82.67	37.85	81.33	38.97	79.95	40.04	78.54	41.06
8	82.63	37.89	81.28	39.00	79.90	40.07	78.49	41.09
0	82.58	37.93	81.24	39.04	79.86	40.11	78.44	41.12
2	82.54	37.96	81.19	39.08	79.81	40.14	78.39	41.10
4	82.49	38.00	81.15	39.11	79.76	40.18	78.34	41.19
6	82.45	38.04	81.10	39.15	79.72	40.21	78.30	41.22
8	82.41	38.08	81.06	39.18	79.67	40.24	78.25	41.26
0	82.36	38.11	81.01	39.22	79.62	40.28	78.20	41.29
2	82.32	38.15	80.97	39.26	79.58	40.31	78.15	41.32
4	<b>82</b> . <b>27</b>	38.19	80.92	39. <b>2</b> 9	79.53	40.35	78.10	41.3
6	82.23	38.23	80.87	39.33	79.48	40.38	78.06	41.39
B	82.18	38.26	80.83	39.36	79.44	40.42	78.01	41.42
0	82.14	38.30	80.78	39.40	79.39	40.45	77.96	41.45
=0.75	0.68	0.31	0.68	0.32	0.67	0.33	0.66	0.38
=1.00	0.91	0.41	0.90	0.43	0.89	0.45	0.89	0.40
= 1.25	1.14	0.52	1.13	0.54	1.12	0.56	1.11	0.5

Table AII-3.—Stadia Reduction—Continued

	25	3•	29	•	30	)• 
Minutes	Hor.	Diff.	Ног.	Diff.	Hor.	Diff.
	dist.	elev.	dist.	elev.	dist.	elev.
0	77.96	41.45	76.50	42.40	75.00	43.30
2	77.91	41.48	76.45	42.43	74.95	43.33
4	77.86	41.52	76.40	42.46	74.90	43.36
6	77.81	41.55	76.35	42.49	74.85	43.39
8	77.77	41.58	76.30	42.53	74.80	43.42
0	77.72	41.61	76.25	42.56	74.75	43.45
2	77.67	41.65	76.20	42.59	74.70	43.47
4	77.62	41.68	76.15	42.62	74.65	43.50
B	77.57	41.71	76.10	42.65	74.60	43.53
8	77.52	41.74	76.05	42.68	74.55	43.56
0	77.48	41.77	76.00	42.71	74.49	43.59
2	77.42	41.81	75.95	42.74	74.44	43.62
4	77.38	41.84	75.90	42.77	74.39	43.65
B	77.33	41.87	75.85	42.80	74.34	43.67
B	77.28	41.90	75.80	42.83	74.29	43.70
0	<b>7</b> 7. <b>2</b> 3	41.93	75.75	42.86	74.24	43.73
2	77.18	41.97	75.70	42.89	74.19	43.70
4	77.13	42.00	75.65	42.92	74.14	43.79
6	77.09	42.03	75.60	42.95	74.09	43.82
8	77.04	42.06	75.55	42.98	74.04	43.84
0	76.99	42.09	75.50	43.01	73.99	43.87
2	76.94	42.12	75.45	43.04	73.93	43.90
4	<b>76.89</b>	42.15	75.40	43.07	73.88	43.93
6	76.84	42.19	75.35	43.10	73.83	43.98
8	76.79	42.22	75.30	43.13	73.78	43.96
0	76.74	42.25	75. <b>2</b> 5	43.16	73.73	44.0
2	76.69	42.28	75.20	43.18	73.68	44.0
4	76.64	42.31	75.15	43.21	73.63	44.0
6	76.59	42.34	75.10	43.24	73.58	44.09
8	76.55	42.37	75.05	43.27	73.52	44.1
0	76.50	42.40	75.00	43.30	73.47	44.1
C=0.75	0.66	0.36	0.65	0.37	0.65	0.38
C=1.00.	0.88	0.48	0.87	0.49	0.86	0.51
= 1.25.	1.10	0.60	1.09	0.62	1.08	0.6

#### APPENDIX III

### SAMPLE SURVEY FIELD NOTES

The field notes contained in this Appendix are presented to show you, the EA2 survey party chief or the EA1 supervisor, how a series of notes are indexed and arranged in a field notebook For completeness, the field notes shown in appendix V of the EA3 TRAMAN are repeated in this Appendix.

The field notes in this Appendix are samples of the types of notes that are kept in surveying. They are not intended to describe how the notes should be kept. That is up to you. You are the one who decides what minimum information is necessary to achieve complete notes, and you are the one who decides how that information is to be recorded. As you are well aware, note keeping is not only an art that makes your notes clean and legible but it is also a science that makes your notes meaningful and correct.

Figures AIII-1 and AIII-2 are samples of the front page and index of a notebook. The front page should be filled out as required by your unit. A separate book should, when possible, be kept for each major project. The index should show all surveying projects by page number and must be kept up-to-date at all times.

An example of recording horizontal measurements is shown in figure AIII-3. To record taping problems, record distance measured (by parts of tapes, if measured) going from one station to the next. Record in the direction in which measured; that is, down for forward measurements, up for backward measurements.

A page check of a direct-level circuit is shown in figure AIII-4. As you recall, when page checking you are determining that the difference between the sum of the backlights and the sum of the forsights is equal to the difference in elevation between the initial benchmark or turning point and the final benchmark or turning point. For direct-level notes exceeding one page, the page check should always be made for each separate page of the notes. The final page should, in addition, show also a check from start to finish of the entire circuit. Remember, too, that when making a page check, you are checking only the accuracy of the arithmetic, not the accuracy of the level shots.

Figure AIII-5 shows horizon closure for a traverse station. In this example, each angle was repeated twice,

once direct and once reverse, using the procedures you studied in chapter 13 of the EA3 TRAMAN for measuring angles by repetition.

Turn all angles, direct and reverse, to the right. Enter means, and if mean does not match single reading to  $\pm 30$ ", reshoot the angles. Never proceed to the next station until horizon closure (360°  $\pm 30$ ") has been achieved.

Figures AIII-6 and AIII-7 show, respectively, notes for a station-angle traverse and a deflection-angle traverse.

## DEPARTMENT OF THE NAVY TY FIRST NAVAL CONSTRUCTION REG

THIRTY FIRST NAVAL CONSTRUCTION REGIMENT NMCB FOUR

# EEVEL, TRANSIT, AND GENERAL SURVEY RECORD BOOK

PORT HUENEME, CALIFORNIA

BLDG & ROAD LAYOUT, NORTH DRIVE.

800K 2 of 4

THEODOLITE WILD T 16

EA2 W. J. BROWN
CHIEF OF PARTY

IMPORTANT

On the opposite page, print the address to which this ook is to be returned, if lost.

Figure AIII-1.—Front page of a notebook.

746E	T	PRO.	ECT		DATE		LO	CAT	ION		
6	HORIZON	AL TAPINO	- TRA	V 27-A	ISJAN 84	S. PRIVE	POR		NEME	CALIF	DRNIA
10	T				12.JAN 84	PI AREA		-11	-		
//		CLOSURE	<u> </u>		25.IAN 84	AREAK		- 11	-		
17	STATION AN	ì	l	i	15 F.E. B.GY	N. DRIVE		- 11 -			[
18	DEFL ANG	T			17 FEB 84	N. DRIVE		_ // -	<u> </u>		
19	TELANGUL				(13 558.64	PI AREA		-11	-		
20	TRIG ELEV			T	15 FFB 64	PI AREA		11 -	-		
2/	MC COY AVE	EXT'D -	HOR X C	ONTROL	20553.64	N. DRIVE		~ 11 -	-		
22			HORIZ TA		22 55 864	-n-		- 11	-		
23	-,-	-	OIFF LEVE	IN6	24 FEBBY	-11-		- 11	_		
24	-/-	-	HOR CURV	ELAYOUT	ZOMARE	-11-		-11-	_		
25	-/-		PROF & CR	FCT LEVELS	ZIMIR BY	-11-		-11	1		
26	-1-		PROFLEY (	EWERLINE)	23 MUR BY	~11-		-11	-		
27	-1-		SLOPE S	AKES	30 MAR 84	-11-		-11			
28	BLOG TZ	155 -	BLOG LA	YOUT	I APR 64	S. DRIVE		11-			
29	PLANETAB	VE MAPP	WG PROB	EM	IOAPR 84	N. DRIVE		—ıı -			
										<u> </u>	
	<u> </u>										

Figure AIII-2.—Index.

The set of horizontal angle control notes shown in figure AIII-8 indicates that the instrument was first set up over station 0+00 and indexed on point No. 1. The horizontal angle (to the right) to PI No. 1 was then turned, as well as the horizontal angle to a church steeple. This locates the traverse and ties it to a point that will not be disturbed The instrument was then moved to PI No. 1 and the deflection angle between 0+00 and PI No. 2 was turned (twice), making sure that the angle was recorded with its proper direction: right (R). The instrument was then moved to PI No. 2 and the procedures repeated

The set of horizontal taping notes in figure AIII-9 shows the proper way to tape and record distances between points. The line in question is taped in both directions, showing each distance and the mean distance. The mean distance must be within 1 in 5,000, or third-order accuracy. A good complete sketch is required.

Differential leveling notes are shown in figure AIII-10. When making the page check do not add the foresight for station 0 + 00, as it is a side shot. Also, note that the stadia distance to 0 + 00 has been omitted for the same reason. When making your sketch, you do not need to show the backsight and foresight distances on the sketch-only on the traverse points, and so forth, normally found on a sketch.

Horizontal curve notes (fig. AIII-11) should include all the curve data plus the deflection angles that are to be turned during the layout of the curve. The sketch should be as shown here. All stations that were staked out should be shown and labeled on the sketch.

Profile and cross-section level notes (fig. AIII-12) are best recorded from the bottom to the top of the page. The left-hand side of the notes should contain columns for stations, backsight (+), height of instrument (HI), foresight (-), and elevations. The right side, as shown, has left, center-line, and right columns. The top number

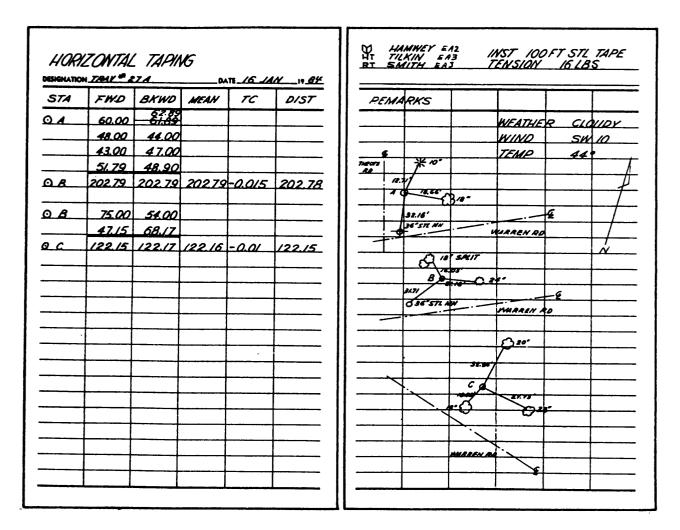


Figure AIII-3.—Horizontal taping.

is the ground elevation at that point, the center number is the rod reading, and the bottom number is the perpendicular distance to the centerline. An additional example of profile levels is shown in figure AIII-13.

Slope-stake notes (fig. AIII-14), as with profile notes, are best recorded from the bottom to the top of the page. As you see in the figure, in addition to grade rod, the right-hand page of the notes has left, center-line, and right columns. In these columns the amount of cut or fill, ground rod, and the distance of the slope stakes from the center line are recorded for each station.

Notes for a building layout are shown in figure AIII-15. Building corner numbers on the sketch must agree with the designation on the left-hand side of the notes. Grade rod setting is computed in the field. Batter elevations are entered in the first column on the right-hand side of the notes—after having been computed at the jobsite. The sketch must show all pertinent data for locating the building.

Typical notes for a plane-table survey are shown in figure AIII-16.

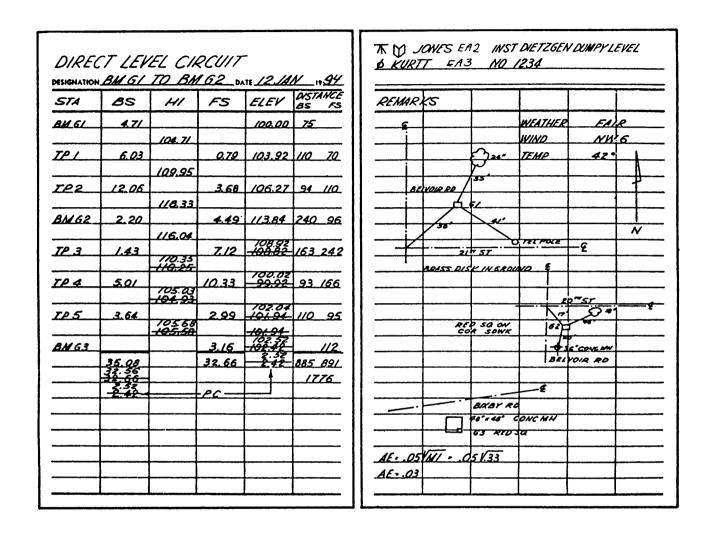


Figure AIII-4.—Page check.

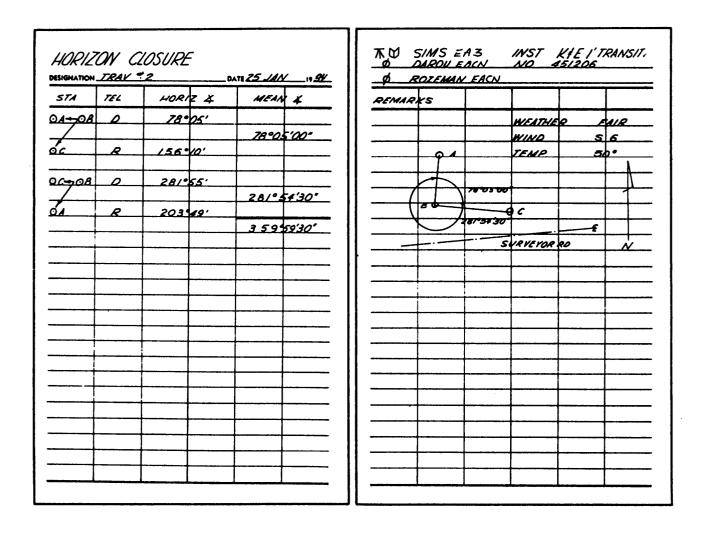


Figure AIII-5.—Horizon closure.

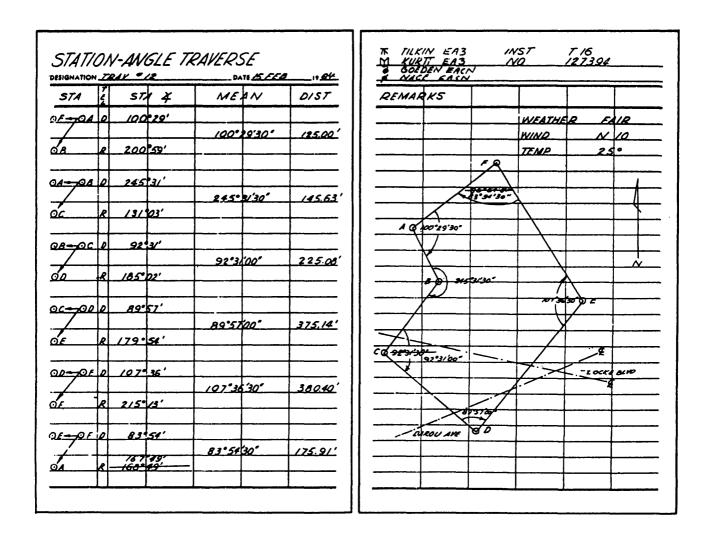


Figure AIII-6.—Station-angle traverse.

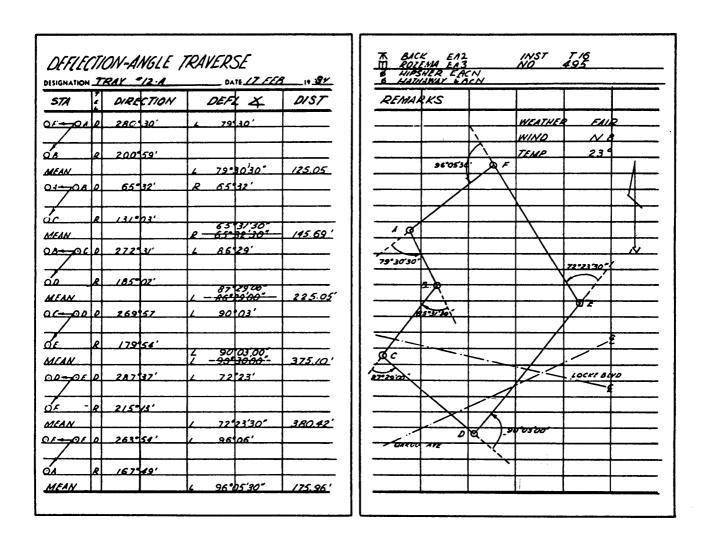


Figure AIII-7.—Deflection-angle traverse.

		NGLE CO. WE EXTEND		TE ZOEE B	1184	M CREW			NO 24	7321	
57A	85	FS	12° X	2º X	MEAN X	REMARK	'S				
0±00	-/				00°00'	RR SPIKE		٩	WEATHER	<u> </u>	EAR
	<del> </del>	01-1	87%6"	174'32'	87%			<del> </del>	MIND	N	<i>B</i>
	101	<del> </del>		<b> </b> -		l	ART 107 70	+	TEMP		
0100	+-/	CHURCH	6/37'	1237/4'	00.00	772 70		0000	64114640	RRI	6/-6
	<del>                                     </del>	STEERLE	6/3/	12374	6/*37'	GMURCH	0776	* ]	IMROX 3	70'	-
		1	ļ	<del> </del>	i			1	277		i
P1 +1	0+00	†	l		00°00'	1		1.			
***************************************		01 02	R 16°10'	R 32°20	R 16.10			4			
								$\mathbf{I}$			
P1 2	PIO	<u> </u>			00.00			000			POLERO
	ļ	POT #2	L 1841'	13772	1.1881			<b>A</b>	-		ļ
	<b></b>	<b> </b>			<del></del>			1870	<del>                                     </del>		
	<del>                                     </del>	<del> </del> -		<u> </u>			/	7_		<del>\i</del>	
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	<del>                                     </del>	<b></b>					12/10		<del>  </del>		<del>                                     </del>
·	<b></b>	1				<del></del>	<del>`                                    </del>		<del>                                     </del>		<del>   </del>
	<b>—</b>										
	1								NOIE: OF	10,201	127
						l	<del></del> j	10505			

Figure AIII-8.—Horizontal angle control.

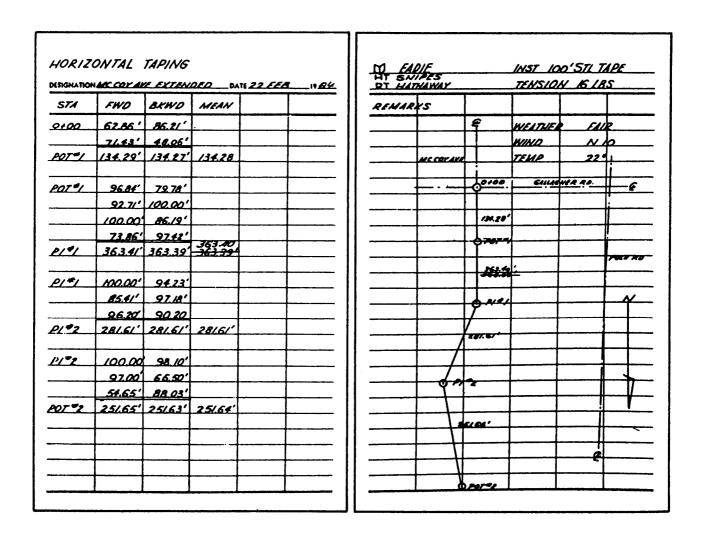


Figure AIII-9.—Horizontal taping between stations.

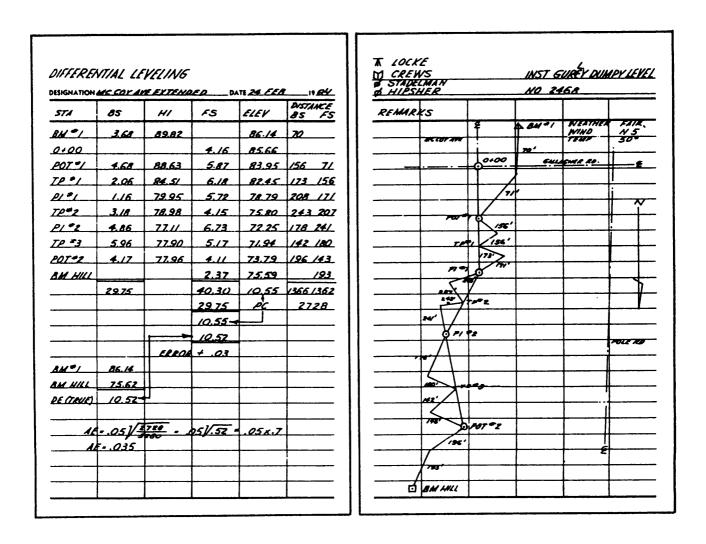


Figure AIII-10.—Differential leveling.

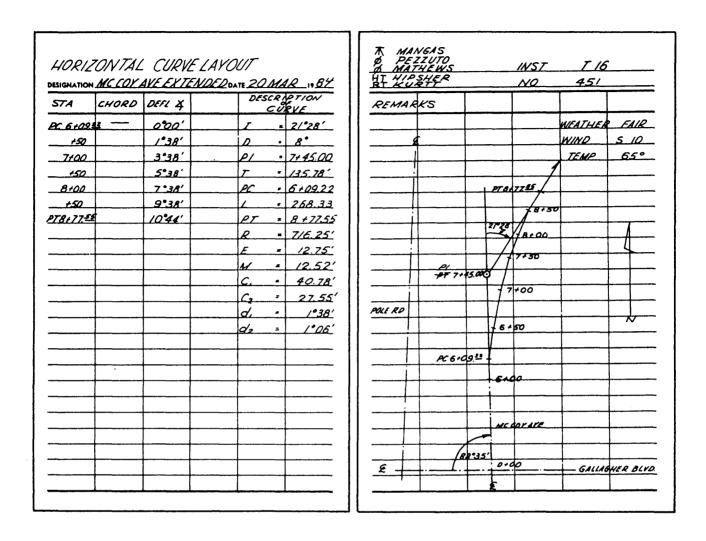


Figure AIII-11.—Horizontal curve layout.

$\begin{array}{c ccccccccccccccccccccccccccccccccccc$		•		TON L	TE ZI MAR		\$ LUFA	KIN		12345		
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	STA	+	HI	_	ELEV			LEFT	٤	`	RIGHT	
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$										WEATHER	FA	IR
(35.0     (33.7     (32.0       3.2     4.5     6.2       30     3.6     3.4       (37.1     (35.9     /34.6     /34.       (1/2     2.3     3.6     3.5       50     2.3     3.6     3.5       (35.1     /34.1     /33.     4.7     4.6       3.0     4.1     4.6     5.0       /32.3     /3.6     5.0     5.0       /32.3     /3.6     5.0     5.0										WIND	s_	p
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$										TEMP	6	<u></u>
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	rp =/			6.08	/32.10							
137							/35.0					132.0
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	7+50			,			30					30
132.3 134.6 133. <u>62</u> 3.6 5. 50	7+00						_/37./ 				/34.6 3.6 20	134 3.5 50
132.3 134.6 133 <u>62</u> 3.6 5. 50							/35./					/33
	6 + 50						<u> 50</u>			<del></del>		30
				-			132.3		/3	6		/33. 5.
134.7 134.6 134.	C 6+0922						30					50
	6400						<u>/34.7</u> <u>3.5</u>	ļ				134.
30	D F UU						_50		<del></del>			30
	6+00	3.02	/38./8									

Figure AIII-12.—Profile and cross-section levels.

	MC COY	AVE EXTE	NDED .	11 23 MA	1R1.59
STA	+	HI		ELEV	TPELEV
BM 4	3.02	/38./8			135.16
0+00		<u> </u>	3.6	134.6	
+2/			5./	/33./	<u> </u>
+50			3.6	134.6	
1100			4.1	134.1	
+50			2.3	/35.9	
<u>+78</u>			4.6	133.6	
2+00			4.5	/33.7	
+50			_6./_	/32./	
3+00			5.8	1324	
4 100			57	132.5	
+10			5.0	/33.2	
_ +60			6.0	132.2	
+76			5.9	1323	
5+00			6.0	132.18	
IP#/	1.79	/33.29	6.68		131.50
6+00			2.3	131.0	
TP=2			4.76		128.53
ł					

TO BACK  SNIPES  SWATHEW		GURLEY DUMPY LEYEY 123
REMARKS		
NAIL IN TREE	60' IFFT OF EN	VEAR O+SO
BOTTOM OF	DIXCH	
	WEATHL	ER FAIR
	WIND	55
	TEMP	60
TOP OF HILL	8 6 STA 6 00	
ON STONE		
	·	

Figure AIII-13.—Additional example of profile levels.

SLOPE esignation a			<i>. NOED</i> a	ATS .30MA	<u>P 1984</u>	<u>dille</u>	PES KIN DELMAN	//VS/	GURLE) DUMPY I	EVEL
STA	+	41	-	ELEV	GRADE ELEV	GRADE ROD	LEFT	<b>\$</b>	RIGHT	
								WEATH	ER CE	OURY
				<del> </del>				WIND		10
				ļ				TEMP		p•
TP ♥/			3.10	/33./0			TOPOF	YUR STA 3+	<i>ao</i>	
				ļ			C 0.3	FOO	F 08	
7+50					132.10	4./	1.0	<del></del>	4.9	
							C 2.0	F / /	F 3.0	
7+00					/32.60	_3.6_	76.0		9/.0	
6+50				<del> </del>	/33./0	3./	C 2.6	F Z Q <u>60</u>	F 4./	
							C 10	F 05	F 15	
C 6+097				<b> </b>	/33.60	2.6	16	3/	4.7	
							F 1.0	F 1.6	F 2.1	
5+00	1.04	/36.20		-	/34./0	2./	12.0	3.7	75.2	

Figure AIII-14.—Slope-stake notes.

ESIGNATION	BLDG		D/	TE / APR	ERADE
STA	<i>8</i> 5	HI	FS	ELEV	ROD
RM 18	5.22	35.22		30.00	
			4.26	30.96	ļ
2			4.14	31.08	
3			4.68	30.54	
			4.52	30.70	
					2.64
2					2.64
3					2.64
4					2.64
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TA SNI D TILK OL LUFA	PES IN IN			KFE LEI KFE L'II	VEL RANSIT
& cow			1219		
BATTER ELEV	REM	IRKS			
			WEATHE	0 4	1/R
			WIND		8
			TEMP	5	20
		COLE B	2000		
	£		20,00	,	
			2000	<i>-</i>	! 1
32.58					
32.58	<b>†</b>				!!
	<del> </del>	<del>                                     </del>			
32.58	<del> </del>	150.00'	7.2055	30.0	<del>71 ~</del>
32.58	<del> </del> -	/30.00			₩
	<del> </del>	<del>  </del>			ROSEANE
		<del></del>			<del>                                     </del>
	ļ	<del>  </del>		<del></del>	₩
	<del> </del>				<del>                                     </del>
	ļ		X.00	<u> </u>	<del>                                     </del>
			<u> </u>		4
·	<u> </u>				<u> </u>
NOTE :	BATTER	POARD E	EVATION	15'11	OVE
	HIGH	EST C	DENER		
	BATTER	BOARD	ELEVATION	DN 15	no e
	1	WOATIO			
	<del></del>		·		

Figure AIII-15.—Building layout.

IGNATION	AREA	<u> </u>	DA	TE <u>LO APE</u>	
STA	CORR H DIST	SCALE	R1	SCALE	PROJ
	625	100	6.25	<u>55</u>	+ 3/
2	160	100	1.60	48	- 3
3	/99	97	2.05	_68	£ 36
4	368	98	3.75	62	+ 45
5	105	100	1.05	54	+ 4
6	425	100	4.25	47	- 12
7	240	98	2.45	37	- 3/
	255	100	2.55	50	0
٥		100	3.65	52	
10		99	0.85	58	
		99	4.55	6/	
		100	2.20	50	
/3		97	2.85	33	<u> </u>
14		100	6.70	54	
		99	3.35	40	
/6	L	99	1.70	3R	
17		100	5.10	47	
		100	4.40	55	<u> </u>

T 200			MO 6666	E ALIDADE	
M SNI			WEATHER WIND TEMP	CLE N 10 75	AR O
RC	DE ±	HI	ELEV	REMAR	es .
	+ 4.3	116.7	112.4	ELEV S	TA B
- 4.6	+ 26.6	ļ	143.3	TOP OF	SLOPE
- 2.8	- 6.0		119.7	BOTTOM	OF SLOPE
- 84	+ 28.5		1452	& RO	10
- 7.2	+ 37.R	L	154.5	E RO	40
- 3.9	+ 0.3		117.0	SPOT E	YEV
- 4.4	- 17.2		99.5	SPOT E	EV
- 7.5	- 39.3		77.4	M.H.	<u> </u>
- 5.4	-5.4		111.3	POWER	POLE
- 6.7				IB" CU	YERT
- 4.3				WATER Y	ALVE
- 7.6				EDGE R	010
- 3./				EDGE R	
- 8.4				EDGE R	DAD
- 5.2	1			COR PIL	K. LOT
- 6.4					K 101
-4./	1			EDGE R	T
- 8.2				18" CUL	
- 5.6	1			POWER	
	1				
	1				
	<del>  </del>				
	<del>  </del>				
	<u> </u>				

Figure AIII-16.—Plane-table notes.

#### APPENDIX IV

#### OTHER USEFUL REFERENCES

**NOTE:** Listed in this Appendix are a few references that you may find useful when assigned to duty outside the Naval Construction Force. They are NOT required study for advancement. Following each reference is a brief description of its purpose.

# Facilities Planning Criteria for Navy and Marine Shore Installations (NAVFAC P-80)

This publication provides planning criteria for determining the requirements for shore-based facilities needed to support Fleet and Marine Corps Operations. In addition, these criteria are used to evaluate the adequacy of existing facilities, to identify facility deficiencies or excesses, and to validate construction project submittals.

#### Facilities Projects Manual (OPNAVINST 11010.20 SERIES)

This instruction provides detailed guidance for the administration of facilities projects at naval shore activities. It includes definitions of the various typesof special projects and the preparation and submittal procedures for special projects.

#### Naval Mobile Construction Battalion Facilities (NAVFAC P80.2)

This publication is similar in purpose to NAVFAC P-80, described above; however, it is tailored specifically to facilities needed to support Naval Mobile Construction Battalion Operations.

#### Shore Facilites Planning Manual (NAVFACINST 11010.44 SERIES)

This instruction explains the process for the planning of shore facilities. It provides guidance on the preparation of Military Construction (MILCON) and Nonappropriated Funded (NAF) project documentation, and for the preparation of site approval documentation required for MILCON, NAF, and special projects.

#### APPENDIX V

# UNIFIED SOIL CLASSIFICATION SYSTEM

The figure and tables in appendix V relate to identification and classification of soil.

 $\label{thm:concerning} \begin{tabular}{ll} Table AV-1 presents useful information concerning the Unified Soil Classification System. \end{tabular}$ 

Figure AV- 1 concerns the classification of soil after the soil has been visually identified as coarse grained, fine grained, or highly organic.

Table AV-2 shows soil characteristics pertinent to roads and airfields.

Table AV-3 shows soil characteristics pertinent to embankments and foundations.

ALL FOLDOUTS REMOVED from APPENDIX V

#### APPENDIX VI

### **ANSWERS**

**NOTE:** This appendix provides answers to the review questions found at the end of each chapter of this TRAMAN. When a question was drawn from a source other than this TRAMAN, the reference source is included with the answer.

#### Chapter 1

- A1. Footing abutment, pile abutment, and concrete abutment.
- A2. The numbers of rows of piles. A bent has one row of piles; a pier has two or more rows.
- A3. Foundation bed, footing, and foundation wall.
- A4. A sheet pile.
- A5. A mole.
- A6. The W12 x 50 wide flange shape. Because it has a greater cross-sectional area.
- A7. The type of construction that uses masonry walls to support floor and roof loads.
- A8. According to Steelworker 3 &2, NAVEDTRA 10653-G, page 12-10, girts are used primarily as attachment members for the metal siding.

#### Chapter 2

- A1. The transmission system and the distribution system.
- A2. The radial distribution system.
- A3. To step down primary voltage to utilization level.
- A4. On a crossarm or spool rack located below the primary mains.
- A5. When they are shown to be more economical or when special circumstances warrant the use of concrete poles.
- A6. Number size, type, voltage, and location.
- A7. The level of underground water that has collected over an impervious stratum.
- A8. Water quantity, reliability, and quality.
- A9. NEVER. Water distribution and sewage collection piping must always be separated.
- A10. To pump sewage from a lower level to a higher level because gravity flow is no longer possible or practical at the lower level.

#### Chapter 3

A1. (A) Traveled way, (B) shoulder, (C) crown, (D) base course, (E) subbase course, (F) surface or surface course.

- A2. Superelevation.
- A3. Final cross sections.

- A1. (A) Architectural, (B) civil (C) mechanical, (D) structural.
- A2. D.
- A3. The roles of the condenser and evaporators can be reversed so that the heat pump can be used for both heating and cooling.
- A4. Temperature, humidity, and air motion. (Source: Utilitiesman 3, NAVEDTRA 12532, page 10-41.)
- A5. Policy and Procedures for Project Drawing and Specification Preparation, MIL-HDBK-1006/1.
- A6. Centimeter. (Source: MIL-HDBK-1006/1.)
- A7. Vertical.
- A8. The letter P. (Source: MIL-HDBK-1006/1.)
- A9. Never.
- A10. To make sure the drawing can be clearly reproduced.

#### Chapter 5

- A1. NAFACENGCOM guide specifications.
- A2. Specifications take precedence over drawings.
- A3. 16.
- A4. Division 2: Site Work
- A5. Part 3: Execution.
- A6. Seabee Planner's and Estimator Handbook, NAVFAC P-405.
- A7. 94 cubic meters.
- A8. 5 percent. (Source: Seabee Planner's and Estimator's Handbook, NAFAC P-405, appendix C.)
- A9. Facilities Planning Guide, NATFAC P-437.
- A10. Volume II, Part 3 (Assemblies).

- A1. The vertical axis.
- A2. Three times.
- A3. To make the line of sight parallel to the horizontal axis of the instrument so that the line of sight will generate a true horizontal plane when the instrument is rotated about the vertical axis.
- A4. To enable you to use any point on the vertical cross hair when you are measuring angles or running lines.
- A5. Only when a low degree of accuracy can be tolerated and an adjustment cannot be made immediately.

- A1. Barometric leveling and trigonometric leveling.
- A2. (A) 398.303 meters, (B) -46.506 meters. (If your answer to Part A is incorrect, then you should review Engineering Aid 3, pages 12-18 and AIII-13.)
- A3. (A) 0.08 feet, (B) no.
- A4. (A) -0.21 feet, (B) +23.02 feet.
- A5. 0 feet.
- A6. 1/959 (or 1/1,000).
- A7. N47°45'E.
- A8. 8,520 square feet.

#### Chapter 8

- A1. Topographic control is the establishment of the horizontal and vertical control points from which the location and elevation of all topographic details are determined.
- A2. 0.05 distance in miles. No.
- A3. (A) 243 feet, (B) +28.1 feet, (C) 202.4 feet.
- A4. (A) 566 feet, (B) 327.3 feet.
- A5. The vertical distance between adjacent contour lines.
- A6. Either a summit or a depression.

#### Chapter 9

- A1. Wingnut B. (Source: Engineering Aid 3, NAVEDTRA 10696.)
- A2. Inside the triangle of error.
- A3. Progression or plane-table traverse.
- A4.  $Correct\ H\text{-}Dist = 365;\ Product = +7.3;\ DE = +0.6;\ Elev = 117.3.$
- A5. For any given area distortion is nearly the same in all directions.
- A6. 3MTV.
- A7. 1,174 miles.

- A1. Reconnaissance, preliminary, and final-location survey phases.
- A2. To make installation, inspection, and maintenance of the line easier and to lessen the requirement for tree trimming.
- A3. The water remaining after absorption, evaporation, and transpiration.
- A4. 95.92 feet.
- A5. (A) 233.3 square feet, (B) 480.7 cubic yards.
- A6. A distance at which the cost of haul equals the cost of excavation.

- A7. (C) The degree of accuracy required.
- A8. 25 feet.
- A9. 0.27974.
- A10. Interior angles.

- A1. Station at  $PC_1$ : 19 + 11.71
  - Station at PI<sub>1</sub>: 23 + 84.28

Station at PCC: 27 + 68.85

Station at PI<sub>2</sub>: 29 + 66.62

Station at  $PT_2$ : 31 + 43.85

- A2.  $d_1 = 1052.1'$ ,  $d_2 = 2°37.9'$ , d = 6°,  $C_1 = 31.13$ fi,  $C_2 = 43.84$ ft, C = 99.81 ft.
- A3. 6 stations (600 feet).
- A4. (A) 124.80 feet, (B) 128.00 feet, (C) 128.80 feet, (D) 128.25 feet, (E) Station 14 + 67, elevation on tune equals 129.0 feet.
- A5. (A) 652.00 feet, (B) 624.00 feet, (C) 636.67 feet, (D) 643.20 feet, (E) Station 11 + 00, elevation = 652.00 feet. (The turning point is the high or low point on a vertical curve. When the tangent grades are equal, the high or low point will be at the center of the tune. When the tangent grades are both plus, the low point is at the PVC and the high point is at the PVT. When both tangent grades are negative, the high point is at the PVC and the low point is at the PVT. When unequal plus and minus tangent grades are encountered, the high or low point will fall on the side of the curve that has the flatter gradient.)

#### Chapter 12

- A1. Electromagnetic EDMs and electro-optical EDMs.
- A2. 729.35 meters.
- A3. Electronic positioning systems.
- A4. The lock mode.

- A1. To determine the moisture content at which the maximum density for a given compactive effort occurs.
- A2. (A) Proctor, (B) 25.
- A3. To ensure that densities obtained in the field conform to the project specification requirements.
- A4. The bulk density can change due to varying temperature and humidity conditions.
- A5. Shear.
- A6. Type V (sulphate-resistant portland cement).
- A7. The aggregate contains exessive organic material.

- A8. Hairline cracking.
- A9. Water that is in excess of the amount needed for a saturated, surface-dry condition.
- A10. For improved watertightness and increased resistance to frost action.
- A11. The chemical reaction between cement and water that causes a concrete to harden.
- A12. When the test specimen breaks outside the middle third of span length by less than 5 percent.
- A13. By heating, dissolution, and emulsification.
- A14. The volubility test.
- A15. A distillation test.

- A1. 75 man-days.
- A2. Indirect labor.
- A3. 61 percent. (Source: NMCB Operations Officer's Handbook, COMSECOND/COMTHIRDNCBINST 5200.2A, Section IV.)
- A4. 150 man-days. (Source: NMCB Operations Officer's Handbook, COMSECOND/THIRDNCBINST 5200.2A, appendix I.)
- A5. Commander, THIRD Naval Construction Brigade.
- A6. So that you can (1) get all of the information needed for the job from the person requesting it and (2) pass this information on to the person to whom you are assigning the job.

#### Chapter 15

- A1. 24.
- A2. 0600.
- A3. The angular distance of a celestial body measured north or south of the celestial equator along the hour circle of the body.
- A4. Over the south celestial pole.
- A5. N43°03′.
- A6. S76°55′00.1"E.
- A7. The calculation of the length of the sides can be cross-checked using different routes.
- A8. A primary triangulation station is used as an instrument station and a sighted station. A secondary station is used only for sighting.
- A9. 38°22′18.25".

- A1. 4.
- A2. True.

- A3. 4.
- A4. (A) 21.18 ercent, (B) 74.25 percent, (C) 4.57 percent, (D) SP.
- A5. (A) LL = 43, (B) PI = 18, (C) CL.
- A6. 4.

Al. (A) 1 1/2 inches, (B) 33.0 gallons, (C) 860 pounds, (D) 1,848 sacks, (E) 333.9 tons.

- A1. Lime.
- A2. Clayey soils.
- A3. Sieve analysis, Atterberg limits test, moisture-density test, and freezethaw test.
- A4. A CBR mold. (Source: NAVFAC MO-330, chapter 5.)

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